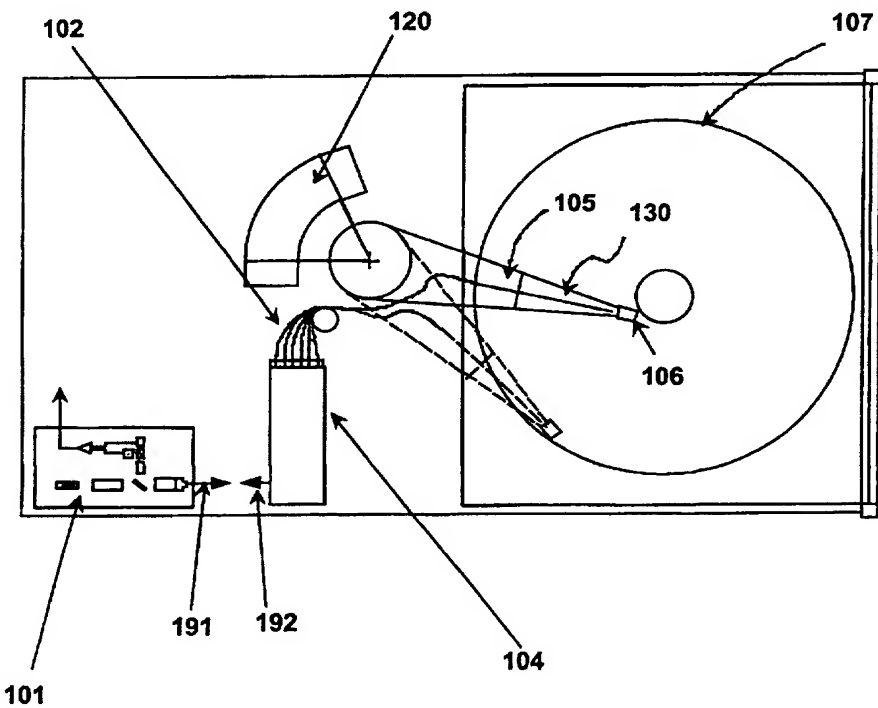


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(54) Title: MAGNETO-OPTICAL DATA STORAGE SYSTEM WITH HIGH CAPACITY		
(57) Abstract A system (100) for maximum magneto-optical data storage is provided. The system (100) utilizes double-sided first surface magnetically-induced super resolution storage media (107) to provide the ability to access a data mark from a plurality of data marks within an optical spot size of an impinging optical beam of light (191).		
100		
		

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MAGNETO-OPTICAL DATA STORAGE SYSTEM WITH HIGH CAPACITY

Background Of The Invention5 1. Field of the Invention

The present invention relates generally to data storage and more particularly to maximum data storage in a magneto-optical data storage system.

2. Background Art

10 Hard disk technology has historically been limited by conventional magnetic head designs. A typical prior art Winchester magnetic storage system includes a magnetic head that has a slider element and a magnetic read/write element and is coupled to a rotary actuator magnet and coil assembly by a suspension and actuator arm so as to be positioned over a surface of a spinning magnetic disk. In operation, lift forces are generated by aerodynamic
15 interactions between the magnetic head and the spinning magnetic disk. The lift forces are opposed by equal and opposite spring forces applied by the suspension such that a predetermined flying height is maintained over a full radial stroke of the rotary actuator assembly above the surface of the spinning magnetic disk.

Flying head designs have been proposed for use with magneto-optical (MO) storage
20 technology. One motivation for using magneto-optical technology stems from the higher areal density capabilities of magneto-optical storage disks. However, despite the historically higher areal storage density available with MO storage technology, the prior art MO disk drive volumetric storage capacity has generally not kept pace with the volumetric storage capacity of magnetic disk drives.

25 One factor that continues to limit MO disk drives is the physical size of the head necessary to hold the various components required for accessing magneto-optical information. Conventional magneto-optical heads, while providing access to magneto-optical disks with areal densities on the order of 1 Gigabit/in², have been based on relatively large optical assemblies, which have made the physical size and mass of the heads rather bulky (typically 3-15mm in a dimension).

30 A number of flying MO head designs incorporating magnetic and optical elements are described in U.S. Patent Number 5,295,122 by Murakami, including: use of free-space alignment of a laser beam with a dynamically moving target, and a number of different configurations of the magnetic and optical elements that are required for reading and writing using the magneto-optical Kerr effect. The large size, mass, and number of elements limits the

minimum head size and, therefore: the speed at which information from the MO disk may be accessed, the tracking bandwidth, and the data density that may be read or written. In the prior art, the large physical size of MO flying heads also limits the spacing between magneto-optical disks to a finite minimum value. Consequently, because the volume available in standard height disk drives is limited, magneto-optical disk drives for use with magneto-optical flying heads have generally not been available as high capacity multi-platter commercial products.

During conventional writing of information in MO disk drives, an incident laser beam heats a selected spot of interest on the MO disk to approximately the Curie point. A time varying vertical bias magnetic field is used to define a pattern of "up" or "down" magnetic domains in a recording layer. Subsequently, as the selected spot of interest cools, information is recorded on the MO disk. The size of the magnetic field that is generated provides a lower limit on a maximum data density that may be recorded on the MO disk. One prior art approach for generating the necessary magnetic field for writing of information has relied on second surface recording techniques. With the second surface recording method, the magnetic field is applied to the spot of interest on the MO disk from a direction opposite that of the incident laser beam. With this approach, only one side of a MO disk may be used.

In addition to the aforementioned limitations, information access in prior art magneto-optical storage systems is limited by the size of the optical spot to which an incident laser beam may be focused on the disk surface. Magneto-optical information access requires the use of polarized laser light for reading and writing information on an MO disk. In the case of reading information, MO technology makes use of a magneto-optical effect ("Kerr" effect) to detect a modulation of polarization rotation imposed on the linearly polarized incident laser beam by the recorded domain marks in the recording layer. The polarization rotation (representing the information stored at recorded marks or in the edges of the recorded marks) is embodied in a reflection of the linearly polarized laser beam and is converted by optics and electronics for readout.

To date, only conventional quadrilayer MO disk structures have been used in commercial MO drives. With conventional MO disks it has not been possible to access information in magnetic domains when the incident laser beam laser beam covers more than one magnetic domain at a time. This limit is substantially proportional to the ratio of the wavelength of the laser beam to the numerical aperture (NA) of the optical elements used. In conventional prior art quadrilayer MO disk structures, therefore, recordation of magnetic domain marks smaller than the minimum incident optical spot size does not provide any benefit.

What is needed, therefore, is an apparatus and method that improves upon prior art access to, and storage of magneto-optical information.

Summary of the Invention

The present invention improves access to and storage of magneto-optical information.

The present invention includes at least one first surface double-sided storage disk in a data

- 5 storage and retrieval system. In the present invention, each surface of the at least one storage disk includes at least one layer. In the present invention, the at least one layer includes a storage layer. In the present invention, the storage layer includes a magnetically-induced super resolution structure. The present invention selectively directs an impinging optical beam to form an optical spot on the storage layer and to record data marks in the storage layer. In the present
- 10 invention, a small size and low profile magnetic coil and yoke improves the ability to record a plurality of small data marks at a high rate and at a short distance from the surface of the storage disk. In the present invention, the plurality of data marks may be recorded within a size of the optical spot. Using the magnetically-induced super resolution structure, the present invention may selectively access within the size of the optical spot a desired one of the plurality of data marks. In the present
- 15 invention, low-profile and low mass optical and magnetic elements may be offset on an optical head to improve access to data stored at an outer periphery and within the magnetically-induced super resolution structure of the at least one magneto-optical storage disk. In the present invention, the optical head includes a low profile and low mass flying magneto-optical head that permits increased volumetric storage capacity of the magneto-optical data storage and retrieval system. In the
- 20 present invention, the flying head includes means for moving an optical element so as to maintain and improve access to information stored on at least one storage disk. The present invention may further include means for independent yet simultaneous access of information stored on a plurality of storage disks.

Brief Description of the Drawings

Figure 1 is a diagram showing a magneto-optical data storage and retrieval system;

Figure 2 is a diagram showing the laser-optics assembly of the magneto-optical data
5 storage and retrieval system of Figure 1;

Figure 3 is a diagram showing a representative optical path that includes the use of a DFB laser source;

Figures 4a-f are diagrams showing the flying magneto-optical head of the magneto-optical data storage in a perspective, a side cross-sectional, an expanded cross-section, a side, a
10 front, a bottom, and a rear view, respectively;

Figure 5 is a diagram showing a representative optical path that includes the use of a RF modulated laser source;

Figure 6 is a diagram showing an embodiment of the GRIN lens;

Figure 7 illustrates an alternative embodiment for the objective optics;

Figure 8 is a diagram showing a magnetic coil assembly in a representative cutaway
15 view;

Figure 9 is a diagram showing a magnetic coil assembly in another representative cutaway view;

Figure 10 is a top view of the conductors of the elongated magnetic coil;

Figure 11 is a diagram of a magneto-optical head used over a surface of a magneto-optical disk;
20

Figure 12 is a diagram illustrating the data tracks that are gained and lost by positioning the objective optics and magnetic coil at a corner of the magneto-optical head;

Figures 13a-c illustrate, a respective perspective section, side section, and exploded side
25 section of the MO disk of the present invention;

Figures 14a-b illustrate a temperature profile of the CAD MSR recording method and a top view of a recording layer, respectively; and

Figure 15 is a diagram illustrating a magneto-optical disk drive.

Detailed Description of the Preferred Embodiments

Referring in detail now to the drawings wherein similar parts of the invention are identified by like reference numerals, there is seen in Figure 1 a diagram showing a magneto-optical data storage and retrieval system. In a preferred embodiment, a magneto-optical (MO) data storage and retrieval system **100** includes a set of Winchester-type flying heads **106** that are adapted for use with a set of double-sided MO disks **107** (one flying head for each MO disk surface). The set of flying heads **106** (hereinafter referred to as flying MO heads) are coupled to a rotary actuator magnet and coil assembly **120** by a respective suspension **130** and actuator arm **105** so as to be positioned over the surfaces of the set of MO disks **107**. In operation, the set of MO disks **107** are rotated by a spindle motor **195** so as to generate aerodynamic lift forces between the set of flying MO heads **106** and so as to maintain the set of flying MO heads **106** in a flying condition approximately 15 micro-inches above the upper and lower surfaces of the set of MO disks **107**. The lift forces are opposed by equal and opposite spring forces applied by the set of suspensions **130**. During non-operation, the set of flying MO heads **106** are maintained statically in a storage condition away from the surfaces of the set of MO disks **107**.

System **100** further includes: a laser-optics assembly **101**, an optical switch **104**, and a set of single-mode PM (polarization maintaining) optical fibers **102**. In the exemplary embodiment, each of the set of single-mode PM optical fibers **102** are coupled through a respective one of the set of actuator arms **105** and suspensions **130** to a respective one of the set of flying MO heads **106**. As will be discussed shortly, the system **100** is used in a configuration that, compared to the prior art, improves access to, and storage of, magneto-optical information.

Figure 2 is a diagram showing the laser-optics assembly of the magneto-optical data storage and retrieval system of Figure 1. In Figure 2, the laser-optics assembly **101** is shown to include a linearly polarized diode laser source **231** operating in a visible or near ultraviolet frequency region and emitting an optical power sufficient for reading and writing using the set of MO disks **107**. In a first embodiment, the laser diode source may be a RF modulated laser source. In a second embodiment, the linearly polarized laser source **231** may be a distributed feed-back (DFB) laser source. In an exemplary embodiment, the linearly polarized laser source **231** is selected to operate within a range 635-685 nm; however, a laser source of other frequencies could also be used. The laser-optics assembly **101** further includes: a collimating

optics **234**, a low wavelength dispersion leaky beam splitter **232**, and a coupling lens **233**. The laser-optics assembly **101** directs (from the linearly polarized laser source **231**) a linearly polarized outgoing laser beam **191** (shown in Figure 1) to the optical switch **104**. The laser-optics assembly **101** further includes: a $\frac{1}{4}$ wave plate **238**, a mirror **235**, and a polarizing beam splitter **232**. In the first embodiment, a linearly polarized reflected laser beam **192** (shown in Figure 1) is directed by the optical switch **104** to the coupling lens **233**, and is routed by the leaky beam splitter **232** to a differential detector comprising: the $\frac{1}{4}$ wave plate **238**, the mirror **235**, and the polarizing beam splitter **239**. In the second embodiment, an optical isolator **297** is included between the laser source **231** and the collimating lens **234**. As is well established in the art, this type of differential detection scheme measures the optical power in two orthogonal polarization components of the reflected laser beam **192**, with a differential signal being a sensitive measure of polarization rotation induced by the Kerr effect at the surface of one of the set of MO disks **107**. In both embodiments, after conversion by a set of photodiodes **236**, the differential signal is processed by the differential amplifier **237** for output as signal **294**. The present invention is not meant to be limited to the aforementioned arrangement of optical elements and sources of light, as other techniques for directing the outgoing laser beam **191** and for detecting the reflected laser beam **192** are well known in the art.

Figure 3 is a diagram showing a representative optical path that includes the use of a DFB laser source. In a preferred embodiment, a representative optical path is shown in Figure 3 to include: the optical switch **104**, one of the set of single-mode PM optical fibers **102**, and one of the set of flying MO heads **106**. The optical switch **104** provides sufficient degrees of selectivity for directing the outgoing laser beam **191** (with reference to laser source **231**) towards a respective proximal end of a respective single-mode PM optical fiber **102**. The outgoing laser beam **191** is further directed by the single-mode PM optical fiber **102** to exit a respective distal end so as to pass through the flying MO head **106** onto a recording/storage layer **349** of a respective MO disk **107**.

In the preferred embodiment the outgoing laser beam **191** is provided by a linearly polarized laser source **231** that is a DFB laser source. A distributed feedback (DFB) diode laser source, unlike an RF-modulated Fabry-Perot diode laser, produces a very narrowband single-frequency output due to the use of a wavelength selective grating element inside the laser cavity. When linearly polarized light from a laser source **231** that is a DFB laser source is launched into a single-mode PM optical fiber **102**, the light exiting the optical fiber includes a polarization state that depends on the relative orientation between the fiber axes and the

incident polarization, and moreover, the output polarization state is very stable in time as long as external perturbations which alter the fiber birefringence are negligible. This behavior is in contrast to that observed with an RF-modulated Fabry-Perot diode laser source which is characterized by high-frequency fluctuations in its spectral output. With a RF modulated laser

5 source, when linearly polarized light is launched into a single-mode PM optical fiber **102**, the laser wavelength fluctuations lead to corresponding polarization fluctuations at the output of the fiber. The resulting polarization noise is minimized when the incident light is launched with its polarization axis aligned with one of the axes of the fiber (discussed below), but even in this case the polarization noise is larger than the corresponding DFB laser case owing to

10 wavelength dependent mode coupling (mode coupling in PM fibers is a phenomenon whereby a small portion of the light that is being guided along one polarization axis is coupled into the orthogonal axis by intrinsic or stress-induced defects). In MO recording it is preferable that the polarization noise be kept to a minimum, such that a SNR in the range of 20-25 dB can be achieved. The present invention identifies that a DFB laser source enables use of the single-

15 mode PM optical fiber **102** for delivery and return of polarized laser light to and from the MO disk **107** while maintaining the aforementioned SNR.

During writing of information, the outgoing laser beam **191** is selectively routed by the optical switch **104** to the MO disk **107** so as to lower a coercivity of the recording/storage layer **349** by heating a selected spot of interest **340** to approximately the Curie point of the

20 recording/storage layer **349**. Preferably, the optical intensity of outgoing laser beam **191** is held constant, while a time varying vertical bias magnetic field is used to define a pattern of "up" or "down" magnetic domains perpendicular to the MO disk **107**. This technique is known as magnetic field modulation (MFM). Alternatively, outgoing laser beam **191** may be modulated in synchronization with the time varying vertical bias magnetic field at the spot of interest **340**

25 in order to better control domain wall locations and reduce domain edge jitter. Subsequently, as the selected spot of interest **340** cools, information is encoded within the recording/storage layer **349** of the respective spinning disk **107**.

During readout of information, the outgoing laser beam **191** (at a lower intensity compared to writing) is selectively routed to the MO disk **107** such that at any given spot of

30 interest **340**, the Kerr effect causes (upon reflection of the outgoing laser beam **191** from the recording/storage layer **349**) a reflected laser beam **192** to have a rotated polarization of either clockwise or counter clockwise sense **363** that depends on the magnetic domain polarity at the spot of interest **340**.

The aforementioned optical path is bi-directional in nature. Accordingly, the reflected laser beam **192** is received through the flying MO head **106** and enters the distal end of the single-mode PM optical fiber **102**. The reflected laser beam **192** propagates along the single-mode PM optical fiber **102** to exit at its proximal end and is selectively routed by the optical switch **104** for transmission towards the laser-optics assembly **101** for subsequent conversion to the signal **294**.

Figures 4a-f are diagrams showing the flying magneto-optical head of the magneto-optical data storage in a perspective, a side cross-sectional, an expanded cross-section, a side, a front, a bottom, and a rear view, respectively. In Figure 4a, the flying MO head **106** is shown for use above a recording/storage layer **349** of one of the set of MO disks **107**. The flying MO head **106** includes: a slider body **444**, an air bearing surface **447**, a quarter-wave plate **493**, a reflective substrate **400**, objective optics **446**, a magnetic coil **460**, and a yoke **462**. The slider body **444** is dimensioned to accommodate the working distances between the objective optics **446**, the single-mode PM optical fiber **102**, and the reflective substrate **400**. The reflective substrate **400** may include a reflective surface which is aligned so as to direct the outgoing laser beam **191** and **192** to and from the recording/storage layer **349**. Although, slider body **444** may include industry standard "mini", "micro", "nano", or "pico" sliders, alternatively dimensioned slider bodies **444** may also be used (as determined by the aforementioned dimensional constraints of the elements used with the flying MO head **106**). Accordingly, in the preferred embodiment, the slider body **444** comprises a mini slider height (889 μm) and a planar footprint area corresponding to that of a nano slider (1600 x 2032 μm).

The single-mode PM optical fiber **102** is coupled to the slider body **444** along an axial cutout **443**, and the objective optics **446** is coupled to the slider body **444** along a vertical corner cutout **411**. Although, in the preferred embodiment the axial cutout **443** is located along a periphery of the slider body, and the vertical cutout **411** is located at a corner of the slider body **444**, the axial cutout **443** and the vertical cutout **411** may be located at other positions on the flying MO head **106**, for example, between the periphery and a central axis or, alternatively, along the central axis itself. Those skilled in the art will recognize that positioning the optical fiber **102** and the objective optics **446** at other than along a central axis may function to affect a center of mass of the magneto-optical head **106** and, thus, its flying dynamics. Accordingly, the point of attachment of the flying MO head **106** to the suspension may require adjustment to compensate for off-center changes in the center of mass of the magneto-optical head **106**. Preferably, the cutouts **443** and **411** may be designed as channels, v-grooves, or any other

suitable means for coupling and aligning the single-mode optical fiber **102** and objective optics **446** to the flying MO head **106**. In the preferred embodiment, the laser beams **191** and **192** traverse an optical path (to and from the recording/storage layer **349** of the MO disk **107**) that includes: the single-mode PM optical fiber **102**, the reflective substrate **400**, the quarter-wave plate **493**, and the objective optics **446**. In the preferred embodiment, the single-mode PM optical fiber **102** and the objective optics **446** are positioned within their respective cutouts to achieve focus of the outgoing laser beam **191** within the spot of interest **340** (Figure 3) as a focused optical spot **448**. The single-mode PM optical fiber **102** and the objective optics **446** may be subsequently secured in place by using ultraviolet curing epoxy or similar adhesive.

As compared to free space delivery of polarized laser light, the single-mode PM optical fiber **102** provides an accurate means of alignment and delivery of both the outgoing **191** laser beam to the reflective substrate **400**, and of the reflected laser beam **192** from the reflective substrate **400** back to the laser-optics assembly **101**. The single-mode optical fiber **102** also provides a low mass and low profile optical path. The low mass of the single-mode optical fiber **102** provides a method of delivering light to the flying MO head **106** without interfering substantially with the operating characteristics of the actuator arm **105** and suspension **130**. The low profile of the single-mode optical fiber **102** provides the ability to reduce the distance between a set of MO disks without interfering with delivery of light or operation of the flying MO head **106**. The single-mode PM optical fiber **102** functions as an aperture of a confocal optical system that has a large depth resolution along its optical axis and an improved transverse resolution. As compared to a non-confocal system, the improved transverse resolution improves the detection of smaller magnetic domain orientations as well as detection of magnetic domain edges. The large depth resolution minimizes cross-talk between closely spaced surface recording levels when using multi-level storage media.

In an exemplary embodiment, the reflective substrate **400** may comprise a steerable micro-machined mirror assembly. The steerable micro-machined mirror assembly **400** includes a small (in one embodiment, less than 300 um square in dimension) reflective central mirror portion **420** (illustrated in Figure 4a by dashed lines representative of the reflective central mirror portion on a side of the steerable micro-machined mirror assembly **400** opposite to that which is visible). The small size and mass of the steerable micro-machined mirror **400** contributes to the ability to design the flying MO head **106** with a low mass and a low profile. As used in the magneto-optical storage and retrieval system **100**, fine tracking and short seeks to a series of nearby tracks may be performed by rotating the reflective central mirror portion **420** about a rotation axis so that the propagation

angle of the outgoing laser beam **191** is changed before transmission to the objective optics **446**.

The reflective central mirror portion **420** is rotated by applying a differential voltage to a set of drive electrodes **404/405** (Figure 4b). The differential voltage on the electrodes creates an electrostatic force that rotates the reflective central mirror portion **420** about a set of axial hinges **410** and enables

5 the focused optical spot **448** to be moved in the radial direction of the MO disk **107**. In the exemplary embodiment, a rotation of approximately ± 2 degrees of the reflective central mirror portion **420** is used for movement of the focused optical spot **448** in an approximately radial direction **450** of the MO disk **107** (equivalent to approximately ± 4 tracks) for storage and retrieval of information, track following, and seeks from one data track to another data track.

10 In other embodiments, other ranges of rotation of the reflective central mirror portion **420** are possible. Coarse tracking may be maintained by adjusting a current to the rotary actuator magnet and coil assembly **120** (Figure 1). The track following signals used to follow a particular track of the MO disk **107** may be derived using combined coarse and fine tracking servo techniques that are well known in the art. For example, a sampled sector servo format
15 may be used to define tracks. The servo format may include either embossed pits stamped into the MO disk **107** or magnetic domain orientations that are read similar to data marks. In the prior art, conventional multiple platter Winchester magnetic disk drives use a set of respective suspensions and actuator arms that move in tandem as one integral unit. Because each flying magnetic head of such an integral unit is fixed relative to another flying magnetic head, during track
20 following of a particular magnetic disk surface simultaneous track following of another magnetic disk surface is not possible. In contrast, irrespective of the movement of the set of actuator arms **105** and set of suspensions **130**, a set of the steerable micro-machined mirror assemblies **400** of the present invention may be used to operate independently and thus permit track following and seeks so as to read and/or write information using more than one MO disk surface at any given time.

25 Independent track following and seeks using a set of concurrently operating steerable micro-machined assemblies **400** would preferably require a set of separate respective read channel and fine track electronics and mirror driving electronics. Because the aforementioned embodiment would also preferably require use of separate laser-optics assemblies **101**, an optical switch **104** for switching between each of the separate optical paths would not necessarily be required.

30 Figure 5 is a diagram showing a representative optical path that includes the use of a RF modulated laser source. In Figure 5 the representative optical path is illustrated with reference to an alternative embodiment, which is shown in Figure 5 to include: the reflective substrate **420**, the quarter-wave plate **493**, the objective optics **446**, and the single-mode PM optical fiber

102. In the alternative embodiment a RF modulated diode laser is used as the laser source **231** (Figure 2). In the alternative embodiment, the single-mode PM optical fiber **102** comprises a first segment **598** coupled to a second segment **599**, each segment comprising a fast axis (Px) and slow axis (Py). The fast axis of the first segment **598** is preferably aligned with the slow axis of the second segment **599**. The outgoing laser beam **191** has an Ox component and an Oy component and is preferably linearly polarized at an angle of approximately 45 degrees relative to the Px and Py axes of the first segment **598**. The quarter-wave plate **493** comprises a fast axis **489** which is preferably aligned in the optical path at an angle of 45 degrees relative to the Px and Py axes of the second segment **599**. In an exemplary embodiment, the quarter-wave plate **493** comprises a square dimension of about 250um, a thickness of about 89um, and a phase retardation of about 90 degrees (+/- 3 degrees) at a wavelength of interest.

Those skilled in the art will recognize that the first and second segments **598** and **599** may be subject to external and/or internal stresses resulting from: mechanical motion, temperature, and pressure; and that, these stresses may affect optical properties of the first and second segments **598** and **599**, for example, their birefringent properties. Accordingly, as the Ox and Oy polarization components propagate through the first and second segments **598** and **599**, the Oy component acquires a shift in phase of ϕ relative to the Ox component. The polarization components Ox and Oy exit the distal end of the second segment **599** and are reflected by the reflective substrate **420** so as to be incident with the surface of the quarter-wave plate **493**. The Ox and Oy components are preferably reflected equally (within 3% of each other) from a gold surface of the reflective substrate **420**. As the Ox and Oy components pass through the quarter-wave plate **493**, the Ox component is converted to a left-hand circular polarization, and the Oy component is converted to a right-hand circular polarization, and the two circular polarizations sum to preferably be an outgoing linear polarization having a polarization angle that depends on the phase shift ϕ . The outgoing linear polarization is reflected from the MO disk **107** and is rotated by the Kerr effect so as to return with a net phase shift between the circular polarization components equal to $\phi + \Delta$, where Δ is a phase shift introduced by the Kerr effect. The reflection from the MO disk **107** reverses the sense of each circular polarization (i.e., left-hand becomes right-hand and vice-versa), such that, upon a second pass through the quarter-wave plate **493**, the right-hand component is converted to a linear polarization component Tx, and the left-hand component is converted to a linear polarization component Ty. The Tx and Ty polarization components of the reflected laser

beam **192** are preferably rotated 90 degrees with respect to the Ox and Oy polarization components of the outgoing laser beam **191**, and the Tx component exhibits a phase shift of $\phi + \Delta$ relative to the Ty component. In an exemplary embodiment, in which the optical transit time through the PM optical fiber is less than 5ns, the birefringence of the PM optical fiber will not change appreciably; thus, as the Tx polarization component of the reflected laser beam **192** propagates back through the second and first segments **599** and **598**, the Ty component acquires an additional phase shift of ϕ with respect to the Tx component. In this manner, after exiting the proximal end of the first segment **598**, the Ty polarization component of the reflected laser beam **192** is phase shifted relative to the Tx polarization component, preferably by only the Kerr phase Δ . The polarization state that emerges from the fiber is elliptical and is converted by the quarter-wave plate **238** of laser-optics assembly **101** to preferably have a linear polarization with a polarization angle proportional to Δ . Subsequently, the linear polarization is detected and converted so as to represent the information stored at the spot of interest **340** as the output signal **294**. Although the present invention minimizes the effects of birefringence introduced by the first and second segments **598** and **599**, the quarter-wave plate **493** also minimizes phase shifts introduced by the optical properties of the reflective surface of the reflective substrate **420**. Additionally, although the quarter-wave plate **493** is disclosed to be positioned in the optical path after the reflective substrate **420**, in an alternative embodiment, the quarter-wave plate **493** may be positioned between the objective optics **446** and the MO disk **107**.

The present invention recognizes that use of a laser source **231** that comprises a RF modulated laser diode may reduce the effects of optical feedback of the reflected laser beam **192** to the laser diode. Those skilled in the art will recognize that RF modulated diodes do not operate at a single wavelength, but rather, as a source of laser light having multimode spectral characteristics (typically with a 10nm bandwidth) and that for each λ , the corresponding phase shift may be minimized by specifying the quarter-wave plate **493** to operate over the bandwidth of the laser source **231**. However, those skilled in the art will recognize that when the Ox and Oy components of the outgoing laser beam **191** are not optimally aligned at 45 degrees relative to the Px and Py axes of the first segment **598**, and/or the quarter-wave plate **493** is not exactly quarter-wave, and/or other optical components in the optical path are not aligned, the phase shift ϕ and, thus, the RF noise components it generates in the output signal **294** may exhibit a dependence on the wavelength fluctuations of the laser source **231**. Accordingly, because in

practice the optical components of system **100** may be aligned to only a limited degree of precision, the wavelength fluctuations of the RF-modulated laser source **231** may function to degrade the signal-to-noise ratio of the output signal **294**.

The present invention identifies that by rotating the fast axis of the first segment **598** orthogonally to the fast axis of the second segment **599**, the RF phase noise created by wavelength fluctuations of the laser source **231** may be canceled in a common mode manner. The first and second segments **598** and **599** may comprise commercially available single-mode PM optical fiber selected to operate at the frequency of interest. The first segment **598** is coupled to the second segment **599** using fusion splicing techniques that are well known in the art, and the fast axis of the first segment **598** is aligned with the slow axis of the second segment **599**, preferably to within an angle of less than .5 degree. Additionally, the first and the second segments **598** and **599** are preferably selected from the same optical fiber manufacturing batch and are preferably of equal length to a precision of less than 1mm. Those skilled in the art will understand that the phase shift encountered by a linearly polarized light propagating with a wavelength λ through each of the first and second segments **598** and **599** is proportional to $2\pi bL/\lambda$ (where b is the birefringence of the PM optical fiber and L is the PM optical fiber length). Therefore, fluctuations in the wavelength λ yield corresponding fluctuations in the phase shift. By aligning the fast axes of the first and second segments **598** and **599** of the PM optical fiber **102** orthogonally to each other and by selecting the two segments **598** and **599** to be approximately equal in length, the present invention identifies that the net birefringence introduced in the optical path by the two segments will be approximately zero and, thus, the phase shift ϕ will be approximately zero and independent of wavelength. In practice, the non-zero net birefringence will be proportional to the difference between the lengths of the first and the second segments **598** and **599**, hence, as compared to the prior art, the RF phase noise in the output signal **294** will be reduced. In the aforementioned alternative embodiment that uses a RF modulated diode laser source **231**, as compared to an embodiment (not shown) in which a continuous one meter in length PM optical fiber is used in place of the first and second segments **598** and **599**, the signal-to-noise ratio of the output signal **294** is reduced approximately 40dB.

Figure 6 is a diagram showing an embodiment of the GRIN lens. In the preferred embodiment, the objective optics **446** includes a micro plano-convex GRIN lens (Graded Index) lens of a non-conventional design that provides a high effective NA, low size, and low

mass single-element objective optics for use with the flying MO head **106**. The non-conventional design of the GRIN lens **446** derives from the radius of curvature that is applied to one plano-surface of a very small diameter conventional plano-plano GRIN rod lens. In the preferred embodiment, this goal is achieved by polishing a conventional plano-plano GRIN rod lens so as to provide a convex surface at planar end of the GRIN rod lens. In the preferred embodiment shown in Figure 6, the objective optics **446** is a cylindrical plano-convex GRIN lens that includes at a bottom end a plano surface and at an opposite end a convex surface with a radius of curvature of 190 μm . As compared to the prior art, the cylindrical and planar portions of the GRIN lens **446** improve the ability to align an optical axis of the objective optics **446** relative to the representative optical path passing through the respective cutout **411** (Figure 4f) of the flying MO head **106**. Use of a single optical element GRIN lens **446** also eliminates a prior art requirement for alignment of multiple objective optic elements relative to each other. In an exemplary embodiment, the GRIN lens **446** diameter is approximately 0.250 μm , and the GRIN lens **446** length is approximately 329 μm . An optical path length from a center point of the reflective central mirror portion **420** to the convex surface of the GRIN lens **446** is approximately 435 μm . The single-mode PM optical fiber **102** has an NA of approximately 0.15, and the distal end of the single-mode PM optical fiber **102** is positioned approximately 450 μm from the center point of the reflective central mirror portion **420**. The GRIN lens **446** comprises a gradient index function of $\sqrt{A} = 3.2$, which provides an effective NA of approximately 0.67. In an exemplary embodiment, in which the laser-optics source **231** (Figure 2) operates at a wavelength of 650 nm, over the propagation angle of the outgoing laser beam **191**, and as the reflective central mirror portion **420** rotates, the optical spot **448** is preferably maintained with a full width at half-maximum intensity (FWHM) of approximately 0.54 μm and with a RMS wavefront error of approximately $\lambda/20$ at a point approximately 25 μm below the convex surface of the GRIN lens **446**. The GRIN lens objective optics **446**, therefore, provides a small size and low mass high NA micro-objective element that is easy to align within the flying MO head **106** during manufacture. One exemplary embodiment of a plano-convex GRIN lens has been described above; however, it will be appreciated that the GRIN lens **446** may comprise other geometries.

The objective lens comprising the GRIN lens **446** has been described as a single element objective lens; however, additional objective optics may also be used to enhance the properties of the GRIN lens **446**. For example, the objective optics may include either an aplanatic lens or a solid immersion lens in conjunction with the GRIN lens **446**. Use of an additional lens element may

achieve a larger numerical aperture and hence a smaller focused optical spot size. A smaller spot size would preferably increase higher areal data densities to be written to and read from the MO disk 107. Micro-optic lenses made by molding glass or plastic may also be used in place of the GRIN lens 446.

5 As is discussed above, the present invention uses objective optics 446 that are manufactured to very small dimensions. The optical and geometrical properties of the objective optics 446 permit the mounting of a small diameter and low profile magnetic coil 460 and yoke 462 on a bottom surface of the flying MO head 106 or, alternatively, on or near the surface of the objective optics 446, without interfering with the aerodynamic flying qualities of the flying
10 MO head 106.

Figure 7 illustrates an alternative embodiment for the objective optics. In an alternative embodiment, the objective optics 446 of Figure 4 may include a molded glass bi-asphere design that provides a miniature lens system with high numerical aperture and good off-axis performance. As with the use of the plano-convex GRIN lens above, use of a single optical element bi-asphere
15 objective optics 446 also eliminates the prior art requirement for alignment of multiple objective optic elements relative to each other. In an exemplary embodiment, the asphere lens 446 diameter is approximately .250 um, and the asphere lens 446 length is approximately 230 um. An optical path length from a center point of the reflective central mirror portion 420 to the top aspherical surface is approximately 514 um. The single-mode PM optical fiber 102 has an NA
20 of approximately .15, and the distal end of the single-mode PM optical fiber 102 is positioned approximately 268 um from the center point of the reflective central mirror portion 420. The top and bottom surfaces of the bi-asphere objective optics 446 are rotationally symmetric to be aspherical as defined by the equation $z = (r^2/R) / (\sqrt{1 - (K - 1(r/R)^2)}) + A_4 r^4 + A_6 r^6$, where for the top surface approximate values for $R = -.1089$ mm, $K = -.8484$, $A_4 = -13.739$ mm⁻⁴, and
25 $A_6 = 490.5349$ mm⁻⁶, and where for the bottom surface approximate values for $R = .1069$ mm, $K = -15.9267$, $A_4 = -13.8907$ mm⁻⁴, and $A_6 = 372.965$ mm⁻⁶. With a preferable index of refraction of 1.605, the effective NA of the bi-asphere objective optics 446 is approximately .68. In an exemplary embodiment in which the laser-optics source 231 (Figure 2) operates at a wavelength of 635 nm, over the propagation angle of the outgoing laser beam 191 and as the
30 reflective central mirror portion 420 rotates, the optical spot 448 is preferably maintained with a full width at half-maximum intensity (FWHM) of approximately 0.52 um and with a RMS wavefront error of approximately $\lambda/20$ at a point approximately 60.5 um below the convex surface of the bi-asphere objective optics 446.

In another embodiment, the objective optics **446** may comprise a molded plastic lens (not shown). If a molded plastic lens is used, the index of refraction of the plastic lens may vary over a desired operating temperature range. Use of a plastic molded lens may require use of a temperature maintaining means on the flying MO head **106**. The means for maintaining a temperature may include a small heater coil surrounding the molded plastic lens. In yet another embodiment, a single molded spherical lens with low numerical aperture (0.2 - 0.4) may be used in conjunction with an aplanatic or solid immersion lens to yield an optical focusing system with relatively high numerical aperture (greater than 0.6). From a manufacturing perspective, molded lenses are attractive because they can be produced in high volume at low cost. One method disclosed here for mass production involves molding a lens array and subsequently sectioning of the array by diamond saw cutting or laser cutting to obtain individual lenses.

Figures 8 and 9 are diagrams showing a magnetic coil assembly in two representative cutaway views. In a preferred embodiment, the magnetic coil **460** is a planar micro-coil that includes a conductor **861**, which is coiled and housed at least partly within a yoke (or

permeable flux guide) **462**, and encapsulated within an insulation layer **816**. In a preferred embodiment, the insulation layer **816** includes a suitable dielectric material, such as a photo-resist material. Although, in the preferred embodiment, the magnetic coil **460** and yoke **462** may be formed on a suitable dielectric protective layer **859**, it is understood that use of the magnetic coil assembly of the present invention without a protective layer **859** is also possible.

The protective layer **859** preferably includes an aperture formed sufficiently wide for ensuring passage of the outgoing **191** and reflected **192** laser beams (Figure 1) through a central passage **823** defined by a sloped portion of the yoke **462**. The sloped portion of the yoke **462** extends (through a plane defined by at least one layer of the conductor **861**) towards the central passage **823**, terminating at a tip portion **829** of the protective layer **859**. In another embodiment, the magnetic coil **460** and yoke **462** may be partly encapsulated within an overcoat (not shown) for added protection and insulation.

In the preferred embodiment the yoke **462** enhances a magnetic field created by the magnetic coil **460** at the recording/storage **349** layer of the MO disk **107**. The sloped portion of the yoke **462** preferably further optimizes enhancement of the magnetic field. In an exemplary embodiment, the yoke **462** is made of a ferromagnetic material having a permeability of approximately 2000, for example, a nickel iron alloy (NiFe), and the yoke ranges in thickness from approximately 4 μm to approximately 6 μm . In one embodiment, the yoke tip **828** terminates at the upper surface of the protective layer **859** such that a maximal magnetic field is

preferably generated by the magnetic coil **460** at or near a point (B) within the recording/storage layer **349** of the MO disk **107** (Figure 9 illustrates the magnetic field lines with dashed lines).

As shown in Figure 4c, the magnetic coil **460** and the yoke **462** are mounted horizontally near the air-bearing surface **447** at, or in proximity to, the lower surface of the objective optics **446** and are centered with respect to an optical axis of the objective optics **446**. The conductor **861** may comprise a suitable conductor, such as copper, that is coiled to comprise between 15 to 40 turns or, preferably, 21 turns. Preferably, the magnetic coil **460** includes two layers spaced apart in a vertical direction by approximately 6 μm . It is understood, however, that in other embodiments, fewer or greater numbers of layers, vertical spacings other than 6 μm , as well as fewer or greater numbers of turns are possible. In an exemplary embodiment, a cross-sectional area of the conductor **861** may vary between approximately 2 μm and 7 μm . In a more specific embodiment, a cross-sectional geometry of the conductor **861** includes a height of approximately 3 μm and a width of approximately 2 μm . It should be understood that other cross-sectional geometries for the conductor **861** are possible, for example, circular or square cross-sections.

In the preferred embodiment, the magnetic coil **460**, the coiled conductor **861**, and yoke **462** include a generally elongated geometry. More specifically the magnetic coil **460** (hereinafter referred to as an elongated magnetic coil), the coiled conductor **861** and yoke **462** include an elliptical geometry. In an exemplary embodiment, the outermost dimension of the conductors **861** along the major axis of the elongated magnetic coil **460** is less than approximately 150 microns and along the minor axis less than approximately 120 microns, and the innermost dimension of the conductor **861** along the major axis of the elongated magnetic coil **460** is less than approximately 50 microns and along the minor axis less than approximately 40 microns. In the exemplary embodiment, an innermost dimension of the yoke **462** along the major axis of the elongated magnetic coil **460** is less than approximately 25 microns and along the minor axis less than approximately 20 microns.

Compared to a circular magnetic coil that includes inner and outer dimensions that are equivalent to the inner and outer dimensions of the elongated magnetic coil **460** along the major axis, the elongated magnetic coil **460** provides an advantage in z-axis magnetic field generation efficiency and self-inductance that is better optimized with respect to the required function of moving the optical spot **448** in the disk radial direction **450** by means of the range of motion of the reflective central mirror portion **420** during fine tracking and short seeks to adjacent tracks of a

MO disk **107**. The elongated magnetic coil **460** geometry provides a denser magnetic field at the surface of the MO disk **107** than would be possible with the aforementioned circular coil. In the preferred embodiment, use of the elongated magnetic coil **460** in combination with the yoke **462** further enhances the magnetic field, preferably, by a factor of approximately two.

- 5 The low profile and low mass of the elongated magnetic coil **460** and associated yoke **462** minimize interference with the aerodynamic flying qualities of the flying MO head **106** such that the flying MO head **106** and, therefore, the elongated magnetic coil **460** and associated yoke **462** may be positioned close to the MO disk **107**. The small diameter of the elongated magnetic coil **460** and yoke **462** provides further benefit, in that, smaller data marks than the prior art
10 may be recorded.

- An exemplary cross-section of the elongated magnetic coil **460** along constraining linear boundaries at extent of the inner diameter of the conductors **861** and the permeable yoke **462** is illustrated in the cross-section shown in Figure 9. In an exemplary embodiment, the sloped portion of the yoke **462** at an inner diameter is shown in a major axis direction (x-axis) **993** of
15 the elongated magnetic coil **460**. The geometry of the sloped portion is a function of the optical path design as defined by the passage of the outgoing laser beam **191** through the central passage **823** during rotation of the reflective central mirror portion **420** (Figure 4). A different geometry **994** applies in the y-z planes. In the preferred embodiment, even though the outermost diameter of the objective optics **446** is larger than the outermost diameter of the
20 elongated magnetic coil **460**, the elongated magnetic coil **460** and yoke **462** do not interfere with the optical passage of light to and from the MO disk **107**. In an embodiment (not shown) of the elongated magnetic coil **460** with an outer major axis dimension larger than the dimension of the objective optics **446** (as compared to a circular coil that has an equivalent outer dimension) the outer dimension of the elongated magnetic coil **460** along the minor axis
25 would be useful in terms of permitting placement of the offset objective optics **446** as close to a periphery of the flying MO head **106** and, therefore, to increase the number of outer data tracks of a MO disk **107** that may be accessed.

- Although the elongated magnetic coil **460** and yoke **462** have been described to include an elliptical geometry, this geometry may be generalized to other situations in which alterations
30 to the geometry of the elongated magnetic coil **460** and yoke **462** are made to accommodate a range of motion of an optical beam within the central passage **823**, while also maintaining minimum spacing between the turns of the conductor **861** with the associated yoke **462** and the

application point of a maximum magnetic field B. Accordingly, other elongated magnetic coil 460, yoke 462, and conductor 862 geometries are within the scope of the invention; for example, oval, rectangular, etc. In another embodiment, in which the reflective central mirror portion 420 (discussed above) is fixed, a circular elongated magnetic coil 460 and yoke 462 geometry would be beneficial in forming a magnetic field at point B. In the aforementioned embodiment, a vertical geometry for the sloped portion of the yoke 462 would be useful in generating an optimal magnetic field. In the preferred embodiment, an upper surface of the yoke 462 (and therefore the elongated magnetic coil 460) is secured to the objective optics 446 (Figure 4c) by well known techniques, such as adhesive 977. In another embodiment, the elongated magnetic coil 460 and the yoke 462 may be adhesively secured to the bottom surface 487 (Figure 4a) of the slider body 444 by a plurality of pads, 825 and 827 (Only two pads are illustrated).

Figure 10 is a top view of the conductors of the elongated magnetic coil. In the preferred embodiment, the conductor 861 includes two pads 924, 926 for connection to an electrical circuit. The pads 924, 926 are preferably made of gold traces. In an exemplary embodiment, with an applied current of less than 50mA, with an input voltage of less than 12 volts, and with a conductor 861 resistance of less than approximately 22 ohms; the elongated magnetic coil 460 exhibits: a self inductance of less than approximately 200nH, and a capacitance of less than approximately 5pf. In the exemplary embodiment, the magnetic field component in a plane perpendicular to the plane of the MO disk 107 (+/- 15 degrees) is reversible (80% +/- full strength) in a time of 4ns. In the exemplary embodiment, a separation distance between the tip 828 of the yoke 462 and the surface of the MO disk 107 is approximately 5um and 10um such that a magnetic field of about 290 Gauss at point B is generated generally within the boundaries of the optical spot 448 formed by the outgoing laser beam 191. This compares favorably the prior art, which because of their bulky size have required that they be positioned at a distance farther away from the magnetic recording media (i.e., at other than the bottom surface of a head). The prior art magnetic coil to recording media distance, consequently, imposes increased current requirements for generation of equivalent magnetic field densities at a media surface. In contrast, the present invention requires less current to generate an equivalent prior art magnetic field density at the media surface. In addition, due to limitations of self inductance, the increased size and current requirements of the prior art magnetic coils is limited by the rate at which their magnetic field

may be switched. The reduction in size and current provided by the magnetic coil **460** and yoke **462**, therefore, increases the rate at which information may be recorded. The bulky prior art coil designs also contribute to head size so as to impose a limit on the number of heads that may be used within any given vertical spacing. For any given field strength, use of the yoke **462** in combination with the elongated coil **460** permits a smaller and less bulky flying magnetic head **106** geometry to be used.

Figure 11 is a diagram of a magneto-optical head used over a surface of a magneto-optical disk. In an exemplary embodiment, the excursion of the optical spot formed by the GRIN lens objective optics **446** over the recording/storage layer **349** of the MO disk **107** is limited at an outer radius by a requirement that the flying MO head **106** maintain a stable aerodynamic flying height and at an inner radius by mechanical constraints of the magneto-optical (MO) data storage and retrieval system **100** that limit movement of the actuator arm **105**. Accordingly, in the exemplary embodiment, the objective optics **446** may access a maximum usable area of the MO disk **107** that comprises a minimum inner radius r_i that is 26.093 mm and a maximum outer radius r_o that is 63.680 mm. In a preferred embodiment, the MO disk **107** comprises 1406.5 data tracks/mm (e.g., a track pitch of .711 μm), and the flying MO head **106** is oriented over the MO disk **107** at the maximal inner excursion with a skew angle of -13.53 degrees and at the maximal outer excursion with a skew angle of 17.72 degrees (relative to tangential lines drawn at the radial data tracks located at the intersection point of the optical spot formed by the objective optics **446** and the minimum inner and maximum outer radii of the recording/storage layer **349**, respectively). In the preferred embodiment, the areal density over all the MO disk **107** radii is maximized using "zone recording" techniques to achieve an exemplary local area density of approximately 3.6 Gb per square inch. A maximum user data rate at the outer radius of the MO disk **107** comprises at least 120 Mbits/sec (at a rotation rate of approximately 4500 RPM). Those skilled in the art will recognize that the user data rate R_D may be calculated using the relationship $R_D = (v) \times (D_L)$ (where v = disk velocity and D_L = linear bit density of the MO disk **107**). The disk velocity v_o at the outer radius of the MO disk **107** may be calculated using the relationship $v_o = r_o \omega = (63.680 \text{ mm}) \times (2\pi \text{ rad/rev}) \times (4500 \text{ rev/60sec}) = 30.008 \text{ m/s}$. Accordingly, the linear bit density D_L required to sustain the desired maximum user data rate at the outer radius may be calculated using the relationship $D_L = R_D / v_o = (120 \text{ Mbits/sec}) / (30.008 \text{ m/s}) = 3998.9 \text{ bits/mm}$.

Figure 12 is a diagram illustrating the data tracks that are gained and lost by positioning the objective optics and magnetic coil at a corner of the magneto-optical head. Those skilled in

the art will recognize that use of objective optics along a central axis and inward from a periphery of a flying MO head results in data tracks at the outer radius of a respective MO disk that may not be accessed. In the present invention, because the GRIN lens objective optics **446** and the elongated magnetic coil **460** are located towards or at a periphery of the flying MO head **106** (as compared to locating the objective optics **446** inward from the periphery and along a central axis of the flying MO head **106**), the radial data tracks that may be accessed at the outer excursion of the magneto-optical head **106** is offset by approximately an equal number of radial data tracks that are inaccessible at the inner excursion of the flying MO head **106**. The present invention takes advantage of the increased recording capacity of the data tracks at the outer radii, as compared to the recording capacity of the data tracks at the inner radii. As compared to the prior art, by positioning the objective optics **446** and elongated magnetic coil **460** offset from the central axis, the present invention increases the amount of data that may be written and read using the MO disk **107**.

The increase in data that may be accessed from the recording/storage layer **349** of the MO disk **107** may be illustrated by comparing a position of the objective optics **446** and the elongated magnetic coil **460** at a corner of the flying MO head **106** to an objective optics and a magnetic coil positioned along a central axis. In Figure 12, the comparison is illustrated by a perpendicular distance between a tangential line drawn at a radial data track located at the optical spot formed by the objective optics **446** and a tangential line drawn at a radial data track located under point E. In an exemplary embodiment, the objective optics **446** and the elongated magnetic coil **460** are placed .0265 inches off-center from the central axis at a corner of the flying MO head **106**. In the exemplary embodiment, at the maximal outer excursion of the flying MO head **106**, the perpendicular distance between the tangential lines (F and G) may be calculated as $d_o = (.0265 \text{ in}) \times (\cos 17.72 \text{ degrees}) = .02525 \text{ in} = 641.165 \text{ um}$ and at the maximum inner excursion between the tangential lines (H and I) as $d_i = (.0265 \text{ in.}) \times (\cos 13.53 \text{ degrees}) = .025765 \text{ in} = 654.42 \text{ um}$. Accordingly, compared to point E, the placement of the objective optics **446** and elongated magnetic coil **460** at a corner of the flying MO head **106** results in a gain of approximately 902 data tracks at the maximal outer excursion of the flying MO head **106** (e.g., $641.165 \text{ um} / .711 \text{ um/track}$), and a loss of approximately 921 tracks at the maximal inner excursion of the flying MO head **106** (e.g., $654.42 \text{ um} / .711 \text{ um/track}$). In the exemplary embodiment, the data gained with the maximal outer excursion of the flying MO head **106** may be calculated using the relationship $C_o = (902 \text{ tracks}) \times (D_L) \times (2\pi) \times (r_o')$, where r_o' is a mean radius of the recording tracks gained (calculated as $r_o - (.5) \times (641.165 \text{ um}) =$

63.3594 mm), and the data lost with the maximal inner excursion of the MO head **106** may be calculated from the relationship $C_i = (921 \text{ tracks}) \times (D_L) \times (2\pi) \times (r_i')$, where r_i' is a mean radius of the recording tracks lost (calculated as $r_i - (.5) \times (654.42 \text{ um}) = 26.4202 \text{ mm}$).

Accordingly, $C_o = 1.43595 \text{ Gb} = 179.493 \text{ MB}$, and $C_i = .061139 \text{ Gb (Gigabits)} = 76.423 \text{ MB}$

5 (MegaBytes). Compared to objective optics positioned at point E on the magneto-optical head **106**, the exemplary embodiment provides a net gain of 103.070 MegaBytes that may be read and written from the MO disk **107**. Thus, compared to prior art objective optics located along a central axis and inward from the periphery of an MO head (e.g., point F), placement of the objective optics **446** and the elongated magnetic coil **460** at the periphery of the flying MO
10 head **106** provides an increase in the amount of data that may be read and written by the magneto-optical (MO) data storage and retrieval system **100**. Although, the objective optics **446** has been described as being located along a periphery of the flying MO head **106**, in other embodiment, other positions of the objective optics **446** and elongated magnetic coil **460** may also provide improved data access.

15 Figures 13a-c illustrate, a respective perspective section, side section, and exploded side section of the MO disk of the present invention. As was discussed above, the present invention transmits polarized light to and from a set of MO disks **107** using low profile and small mass optical paths. The low profile and small mass optical paths enable the present invention to use a plurality of double sided first surface MO disks **107** with a very small spacing between the
20 disks. Unlike the prior art, the double-sided first surface MO disks **107** of the present invention utilize magnetically-induced super resolution (MSR) film structures. As compared to conventional quadrilayer MO disks, an MSR film structure can support readout of at least one data domain mark within any given optical spot **448** formed by the outgoing laser beam **191** on and MO disk **107** and, preferably a plurality of data domain marks. The MO disk **107** of the
25 present invention uses thermally-induced masking of written magnetic domain patterns in the MSR film structure to enable extension of the modulation transfer function of the readout optical system. In the multi-layered recording/storage layer **349** structure shown in Figures 13a-c, adjacent magnetic layers are coupled by an atomic exchange mechanism to form magnetic apertures, which are smaller than the optical beam size. There are several methods
30 for selecting which magnetic domain within the illuminated area of the disk is selected and presented to the readout beam, mainly front-aperture detection (FAD), rear-aperture detection (RAD), and central-aperture detection (CAD). These methods differ in the location of the domain within the illuminated area of the disk which is selected for display by the reflected laser

beam **192**. In the preferred embodiment, the CAD method is used for selection of a particular magnetic domain; however, it will be appreciated that the invention is not limited to this method. The CAD, FAD, and RAD methods are illustrated and discussed below with reference to Figure 14 below. In these three techniques, data is written onto the storage layer **1371** with the flying MO head **106** flying close to the MO disk **107**, which is modulated using the aforementioned MFM recording techniques. The elongated magnetic coil **460** and yoke **462** (Figure 4c) of the present invention are a very small diameter and, yet, do not interfere with passage of light through the objective optics **446**. The magnetic field created by the elongated magnetic coil **460** can be directed to impinge on a smaller area of the MO disk **107** than the prior art, and, therefore to record data as magnetic domain marks that are smaller than the optical spot **448** size.

In an exemplary embodiment, the MO disk **107** is fabricated as a double sided first surface MSR media that includes storage layers **1364** and **1365**, and embossed pits on opposing sides of a substrate **1366**. Each layer preferably includes a lubricant/protective layer **1367** of a thickness approximately 3nm. In one embodiment, the lubricant/protective layer **1367** may include a thin amorphous carbon film. Preferably, the lubricant/protective layer **1367** includes a transmittance of at least .95. The lubricant/protective layer preferably facilitates dynamic load and unload of the flying MO head **106** to and from the flying condition, and also supports long term stability during track-following and track seeking. The lubricant/protective layer **1367** also provides an anti-static function to keep the MO disk **107** resistivity below $10^{12}/\text{ohms}$. The lubricant/protective layer **1367** is deposited over a silicon nitride (SiN) upper dielectric layer **1368**. Although in an alternative embodiment, the lubricant/protective layer **1367** can provide a protective function, in the exemplary embodiment, the dielectric layer **1368** also serves this function. The upper dielectric layer **1368** includes a thickness typically in the range of 60 - 100 nm. The upper dielectric layer **1368** acts to provide a number of functions, including: (a) a hard protective coating to prevent film damage during disk handling or inadvertent head-disk contact during device operation; (b) thickness, refractive index, and thermal properties that adjust for the reflectance and Kerr effect properties of the layers below; (c) sufficient impermeability to protect and passivate the chemically active MO layers below. The upper dielectric layer **1368** is deposited over a plurality of magnetically active layers **1369** and **1371** that have a total thickness of approximately 40-100 nm. The layers **1369** and **1371** preferably function to yield a readout aperture with a read power of approximately 3 mW. The upper layer **1369** is a read layer and is approximately 40 nm thick to preferably yield a strong

Kerr effect and maximal signal-to-noise performance. In an exemplary embodiment, the upper layer **1369** is a ferrimagnetic material such as GdFeCo. In the exemplary embodiment, the lower layer **1371** is data storage layer comprised of a ferrimagnetic alloy such as DyFeCo having a thickness of approximately 40nm. In both layers **1369** and **1371**, each magnetic data domain consists of a region of the layer that is magnetized in a perpendicular direction to the surface of the MO disk **107**. The upper **1369** and lower **1371** layers preferably have a low transmittance such that an optical reflective function is provided by the layers above. This compares favorably to traditional quadrilayer MO disk media, in that, a separate reflective layer is not necessarily required. The lower layer **1371** is deposited on top of a silicon nitride dielectric layer **1372** that has a thickness of approximately 20 - 40 nm. The lower dielectric layer **1372** is disposed on the substrate **1366**. The thickness of the various layers of the MO disk **107** are preferably selected for proper thermal behavior (appropriate power sensitivity and good temperature gradients for writing and for sharp MSR aperture formation) and for good exchange coupling.

In an exemplary embodiment, the substrate **1366** may be a single piece metal such as Aluminum Magnesium (AlMg) or, for alternatively, a plastic, a glass, a ceramic substrate, or a two-piece laminated plastic substrate. It is understood, however, that other materials for the substrate **1366** are within the scope of the present invention. The substrate **1366** should be sufficiently rigid to resist deformation when the MO disk is spun at 4500 rpm. The substrate **1366** thickness is preferably in a range of 1.20 +/- .05 mm. If a plastic substrate is used, a thermal heat sinking layer may be deposited directly on the substrate **1366** to control lateral heat flow, for example a metallic layer. If a metal substrate is selected, a hard overcoat such as nickel phosphorous (NiP) may be deposited on the substrate **1366** before the deposition of the dielectric layer **1372**. The overcoat should have a sufficiently low thermal conductivity such that it does not degrade the writing sensitivity of the disk (i.e., elevate the writing/reading/erasing power requirement). If a plastic is selected, tracking and format information may be embossed ("hard formatting"). If a metal or glass substrate is selected, mass replicated format features (e.g., photopolymerization) may be used. Alternatively, "soft formatting" by magnetic layer writing may be used.

In an alternative exemplary embodiment, the layers **1369** and **1371** may be separated by a magnetic or non-magnetic coupling layer (not shown) so as to improve exchange coupling. In another alternative exemplary embodiment, the layers **1369** and **1371** may comprise multi-

layers deposited contiguously, or separated by intervening dielectric layers, depending on the interlayer magnetic coupling and resultant MSR performance desired.

Figures 14a-b illustrate a temperature profile of the CAD MSR recording method and a top view of a recording layer, respectively. With the CAD method mentioned above, MSR
5 creates an essentially elliptically shaped aperture **1470** inside of a particular isotherm in the read layer **1369** due to an elevated temperature profile created by the outgoing laser beam **191**. By carefully designing the MO film composition, stack architecture, and thickness, the temperature profile **1483** can be tailored for a desired power sensitivity as well as signal and noise performance. The aperture **1470** includes a high temperature zone in which the net polarization
10 recorded storage layer is copied upward to the read layer **1369**. The copying is a parallel coupling of the perpendicular magnetization (to the disk plane) of a particular data domain mark **1413** in the storage layer **1371** to the magnetization of the read layer **1369**. Near room temperature, the read layer **1369** is magnetized in-plane so as to induce no Kerr effect within the optical spot **448** that would normally be formed by the incident outgoing laser beam **191**.
15 When a magnetization between layers is induced by temperature elevation, a relatively strong Kerr signal is available only for the data mark **1413** not masked by the aperture for the outgoing laser beam **191** incident on the read layer **1369**. The CAD method is advantageous for a number of reasons, including: the aperture shape is easily controlled by the level of readout laser power (typically 2-3 mW); the aperture shape masks not only magnetization
20 information that would otherwise interfere with the data marks to be read along the data track, but it also shields adjacent track information, thus enabling higher track and linear densities; no readout magnetic field is required; and the read layer and write layer structure is relatively simple.

Figure 15 is a diagram illustrating a magneto-optical disk drive. In a preferred
25 embodiment, the magneto-optical system **100** comprises a compact high-speed and high-capacity MO disk drive **1500** that includes an industry standard 5.25 inch half-height form factor (1.625 inch), at least six double-sided MO disks **107**, and at least twelve flying MO heads **106**. As discussed above, the flying MO heads **106** may be manufactured to include optical and magnetic elements that provide a very small mass and low profile high NA optical
30 system so as to enable utilization of at least one double-sided MSR MO disk **107** and preferably a plurality of double-sided MSR MO disks **107** within a small form factor disk drive and; therefore, to comprise a higher areal and volumetric and storage capacity than is permitted in an equivalent volume of the prior art. In the preferred embodiment, a spacing between each of the

at least six MO disks **107** is .182 inches. In an exemplary embodiment, the elongated magnetic coil **460** and yoke **462** enable each side of the MO disk **107** to comprise at least 5 GigaBytes of written data marks. In an exemplary embodiment, the objective optics **446** provides an approximately .54 um optical spot size **448** to enable reading of the data marks. The present invention should not, however, be limited by these specifications as it is understood that in alternative embodiments other spacings between the set of MO disks **107** are possible to achieve other volumetric storage capacities; and with other optical spots sizes and coil and yoke designs, reading and writing of other MO disk **107** areal data capacities.

In an alternative embodiment, the half-height form factor MO disk drive **1500** may include a removable MO disk cartridge portion **1510** and two fixed internal MO disks **107**. By providing the removable MO disk cartridge portion **1510**, the fixed internal and removable combination permits external information to be efficiently delivered to the MO disk drive **1500** for subsequent transfer to the internal MO disks **107**. The copied information may, subsequently, be recorded back onto the removable MO disk cartridge portion **1510** for distribution to other computer systems. In addition, the removable MO disk cartridge portion **1510** allows for very convenient and high speed back-up storage of the internal MO spinning disks **107**. The fixed internal and removable combination also permits storage of data files on the removable MO disk cartridge portion **1510** and system files and software applications on the internal MO spinning disks **107**. In another alternative embodiment (not shown) an MO disk drive **1500** may include: any number (including zero) of internal MO disks **107** and/or any number of MO disks **107** within any number of removable MO disk cartridge portions **1510**.

The present invention may be practiced in many different optical disk drive embodiments, for example: read only optical drives, without use of a yoke, with other form factors, with other optical sources of light, with other types of optical fibers, with other optical elements. For example, the low profile optical paths disclosed by the present invention may be used to convey information to and from a storage location without requiring objective optics (e.g., using a tapered optical fiber or an optical fiber with a lens formed on an end); and/or reflective substrates (e.g., using a curved optical fiber to convey information along surfaces of the magneto-optical head **106**); and/or quarter-wave plates, as in a system that effectuates compensation of PM optical fibers using dynamic phase compensation. Free space optical paths may also be used to deliver and receive laser light, for example, with a suitably aligned laser diode and detector mounted on the actuator arm or, alternatively, on the flying head itself.

The present invention does not necessarily require use of rotary actuator arms, for example, linear actuator arms may be used.

Although the present invention has been described herein with reference to particular embodiments thereof, a latitude of modification, various changes and substitutions are intended
5 in the foregoing disclosure, and it will be appreciated that in some instances some features of the invention will be employed without a corresponding use of other features without departure from the scope of the invention as set forth.

CLAIMS

What is claimed is:

1. An information storage system, said system comprising:
a magnetically-induced super resolution storage medium;
5 a light source;
a head disposed between said storage medium and said light source;
at least one optical element coupled to said head for illuminating said storage medium with a
light from said source and for receiving reflected light from said storage medium; and
magnetic field generating means coupled to said head for controllably generating a magnetic
10 field in a region of said surface of said storage medium that is illuminated by said light.
2. The system of Claim 1, wherein said at least one optical element comprises an objective
optics that has an outer diameter.
3. The system of Claim 2, wherein said magnetic field generating means comprises:
a coil coupled to said at least one optical element, said coil comprising an outer diameter
15 that is smaller than said outer diameter of said optical element.
4. The system of Claim 3, wherein said coil is disposed between said objective optics and
said storage medium.
5. The system of Claim 3, wherein said coil includes a central aperture through which said
light passes.
- 20 6. The system of Claim 2, wherein said head comprises a periphery and wherein said
objective optics is coupled to said head along said periphery.
7. The system of Claim 1, wherein said light source comprises a laser coupled to collimating
optics for producing a collimated light beam.
8. The system of Claim 1, wherein said light source comprises a substantially single
25 frequency source of light.

9. The system of Claim 1, wherein said light source comprises an optical fiber.

10. The system of Claim 1, wherein said at least one optical element comprises an optical fiber.

11. The system of Claim 1, wherein said at least one optical element comprises a steerable
5 mirror.

12. The system of Claim 11, wherein said steerable mirror comprises a micro-machined mirror.

13. The system of Claim 1, wherein said at least one optical element comprises:

a coupling lens disposed in an optical path of the light for focusing said light onto said

10 portion of said storage medium surface;

a quarter wave plate disposed in the optical path; and

further comprising optical detecting means comprising:

a polarizing beam splitter disposed in an optical path of said reflected beam, said polarizing beam splitter splitting said reflected beam into two orthogonally polarized component beams; and

15 a differential detector disposed in the optical paths of said component beams for measuring the power in both components to determine the polarization rotation of said reflected beam.

14. The system of Claim 1, wherein said at least one optical element comprises:

a polarization maintaining optical fiber for conducting said light from said light source;

reflection means disposed in an optical path for directing said light from said polarization

20 maintaining optical fiber toward said storage medium;

a quarter wave plate disposed in said optical path; and

objective optics disposed in the optical path of the light for focusing said light onto said portion of said storage medium surface.

15. The system of Claim 14, wherein said reflection means comprises a steerable mirror,
25 said steerable mirror dynamically varying said optical path.

16. The system of Claim 14, wherein said objective optics comprises a GRIN lens.
17. The system of Claim 16, wherein said GRIN lens comprises a plano-convex lens.
18. The system of Claim 14, wherein said objective optics comprises an aplanatic lens.
19. The system of Claim 14, wherein said objective optics comprises a solid immersion lens.
- 5 20. The system of Claim 14, wherein said objective optics comprises a molded glass bi-asphere lens.
21. The system of Claim 14, wherein said objective optics comprises a molded plastic lens.
22. The system of Claim 14, wherein said objective optics and said magnetic field generating means are disposed at a corner of said head such that an area of said storage medium surface that is
- 10 accessible to said head is increased compared to the accessible surface if said objective optics and said magnetic field generating means were disposed along a central axis of said head.
23. The system of Claim 1, wherein said storage medium includes magnetic domains and whereby said light illuminating said storage medium encompasses a plurality of said magnetic domains.
- 15 24. The system of Claim 1, wherein said storage medium comprises:
- a substrate; and
- at least one layer supported by said substrate, said at least one layer including a surface exposed to said light, said layer containing magnetic material for storing data by means of magnetically induced super-resolution.
- 20 25. The system of Claim 1, wherein said storage medium comprises a plurality of adjacent sublayers, and wherein said adjacent sublayers are coupled by an atomic exchange mechanism.
26. The system of Claim 25, wherein at least one of said sublayers comprises ferrimagnetic material.
27. The system of Claim 26, wherein said ferrimagnetic material is GdFeCo.
- 25 28. The system of Claim 26, wherein said ferrimagnetic material is DyFeCo.

29. The system of Claim 25, wherein said plurality of sublayers comprise:

a storage layer; and

a read layer.

30. The magneto-optical storage system of Claim 29, wherein said plurality of sublayers

5 further comprise an intermediate layer disposed between said storage layer and said read layer for improving exchange coupling between the storage layer and the read layer.

31. The storage system of Claim 23, wherein said magnetic domains are detected by the front-aperture detection method.

32. The system of Claim 23, wherein said magnetic domains are detected by the rear-
10 aperture detection method.

33. The system of Claim 23, wherein said magnetic domains are detected by the central-aperture detection method.

34. The system of Claim 29, wherein said storage layer provides an optical reflective function.

15 35. An information system, said system comprising:

a plurality of magnetically induced super-resolution storage media;

a light source;

optical switching means for controllably directing a light from said light source to one of said storage media

20 at least one head disposed in proximity to a surface of said storage media and

at least one optical element coupled to said head for illuminating said storage medium and for receiving reflected light from said storage media;

optical detection means for detecting optical signals in said reflected light; and

25 magnetic field generating means coupled to said head for controllably generating a magnetic domain mark in a region of said surface of said storage at is illuminated by said light.

36. The system of Claim 35, wherein said light encompasses a plurality of magnetic domain marks.

37. The system of Claim 35, wherein said at least one optical element comprises an objective optics that has an outer diameter.

5 38. The system of Claim 37, wherein said magnetic field generating means comprises:
a coil coupled to said at least one optical element, said coil comprising an outer diameter that is smaller than said outer diameter of said optical element.

39. The system of Claim 38, wherein said coil is disposed between said objective optics and said storage media.

10 40. The system of Claim 35, wherein at least one of said storage media comprises a double-sided magneto-optical disk.

41. The system of Claim 35, wherein at least one of said storage media is removable.

42. The system of Claim 35, wherein said plurality of storage media comprises at least six double sided disks disposed within a half-height form factor.

15 43. The system of Claim 42, wherein a vertical spacing between said disks is approximately .182 inches.

44. A method of passing light between a source and a magnetically-induced super resolution storage medium comprising the steps of:

20 providing a first head in proximity to said storage medium;
providing at least one optical element and a magnetic field generating means coupled to said head;

directing said light using at least one optical element; and

directing said light through said magnetic field generating means.

25 45. The method as recited in claim 44, further comprising a step of providing said light at a substantially single wavelength.

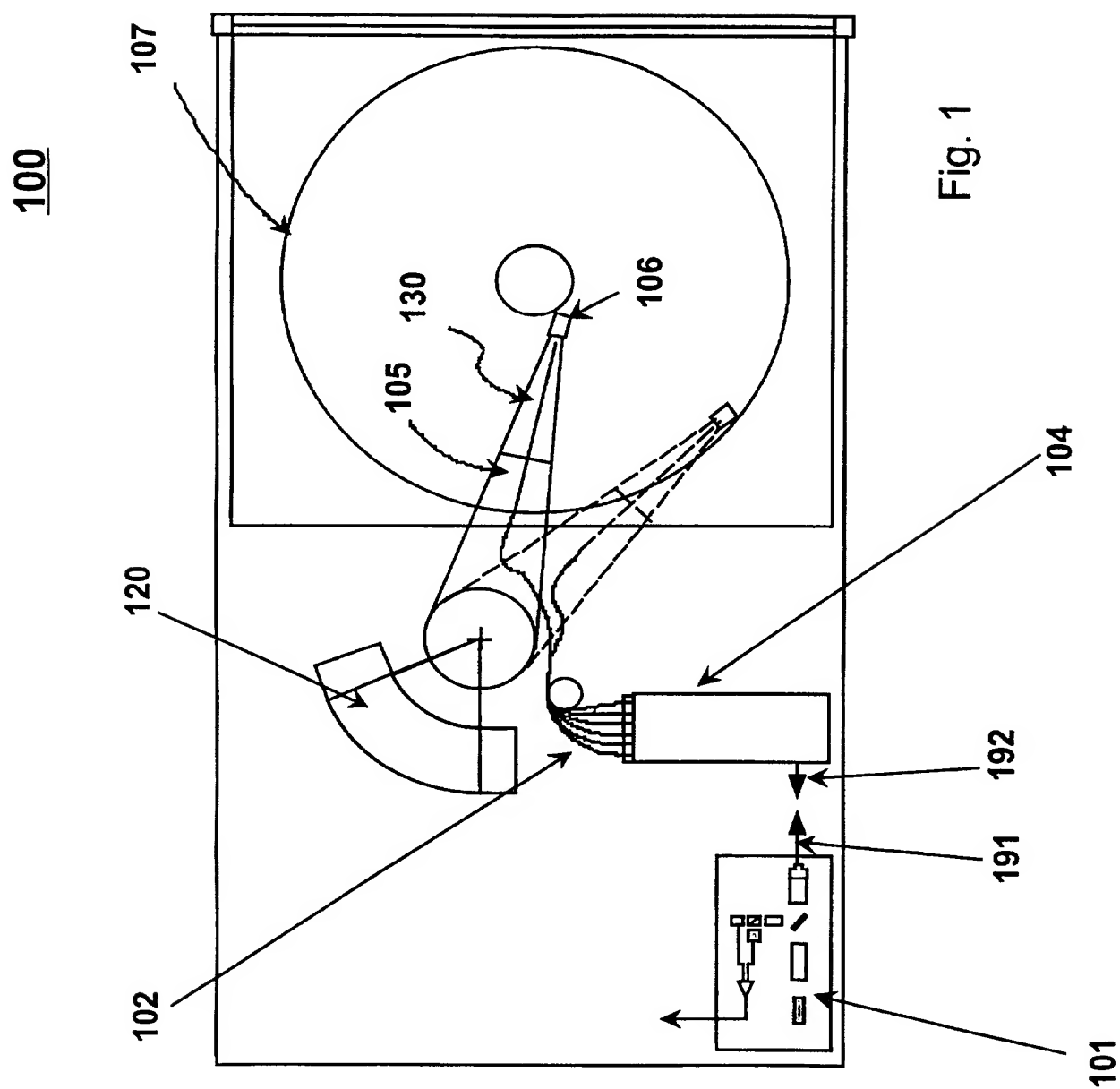
46. The method as recited in claim 44, wherein said step of directing said light using at least one optical element comprises directing said light through an optical fiber.

47. The method as recited in claim 44, wherein said step of directing said light using at least one optical element comprises reflecting said light from a micro-machined mirror.

48. The method as recited in claim 44, wherein said head comprises a periphery and wherein said at least one optical element is coupled to said head along said periphery.

5 49. The method as recited in claim 44, further comprising the steps of providing a second head in proximity to said storage medium and providing at least one optical element and a magnetic field generating means coupled to said second head.

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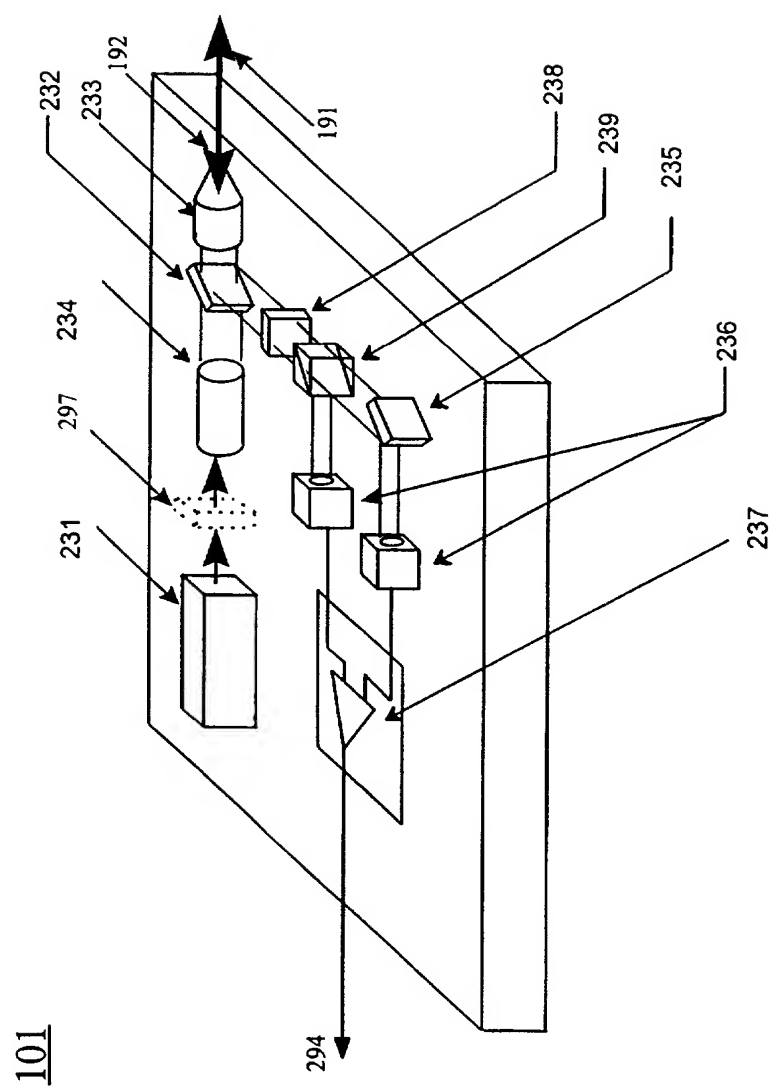


Fig. 2

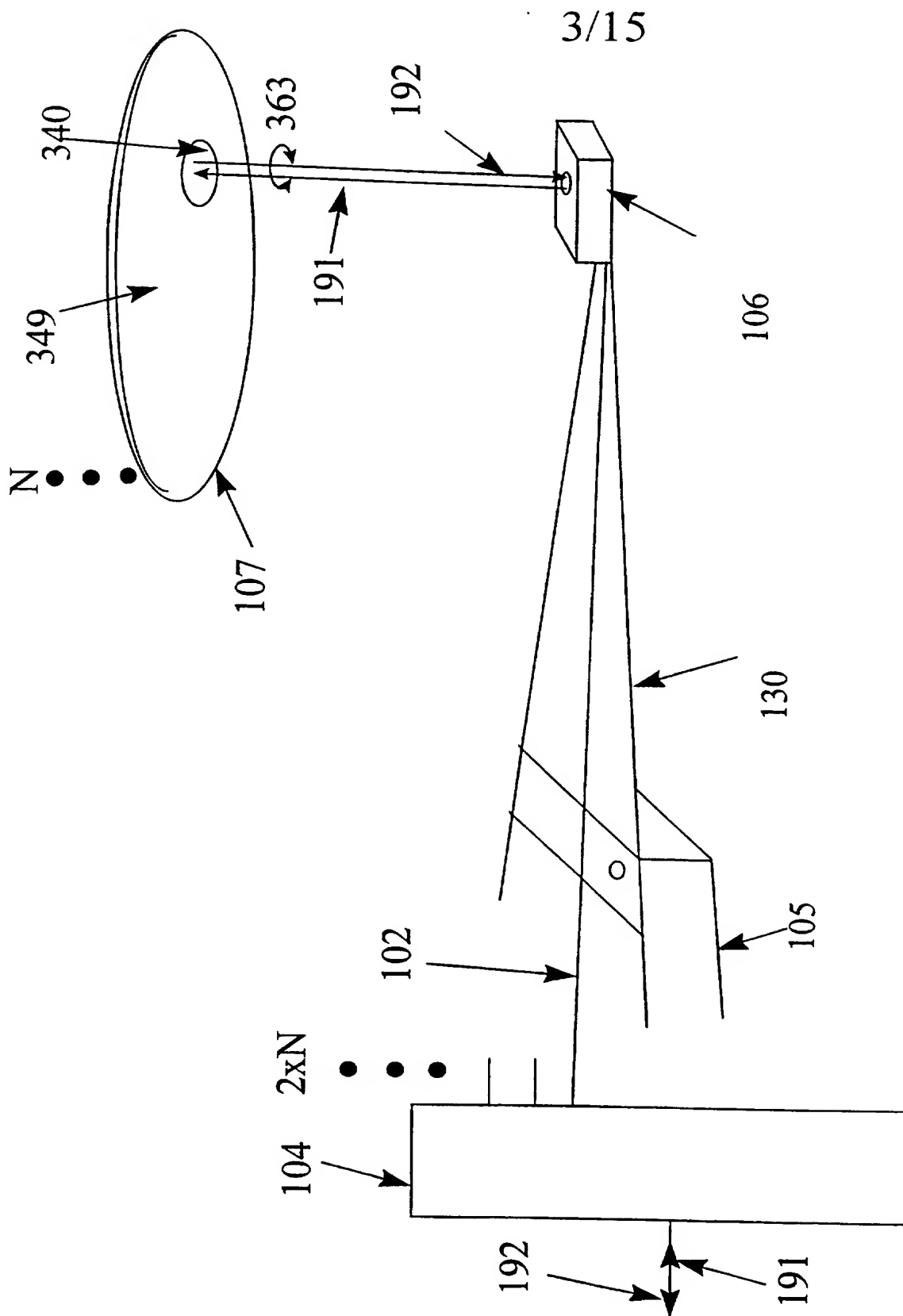


Fig. 3

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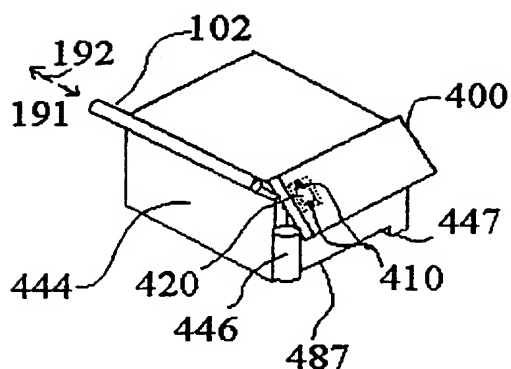


FIG. 4a

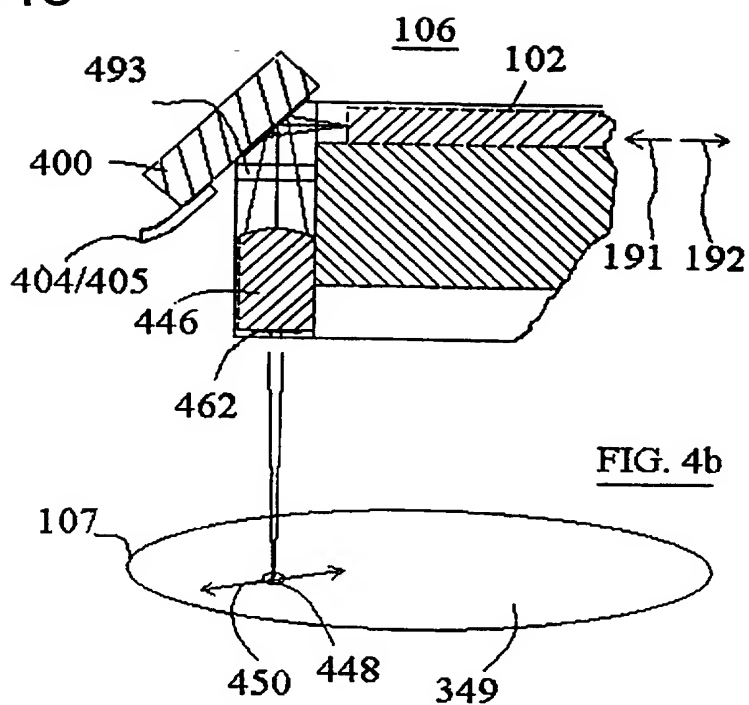


FIG. 4b

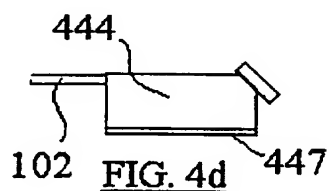


FIG. 4d

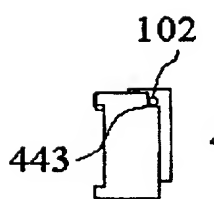


FIG. 4g

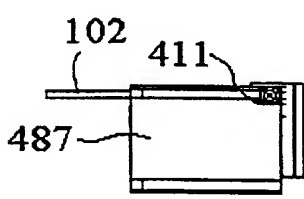


FIG. 4f

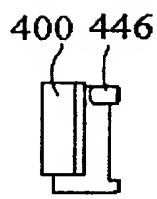


FIG. 4e

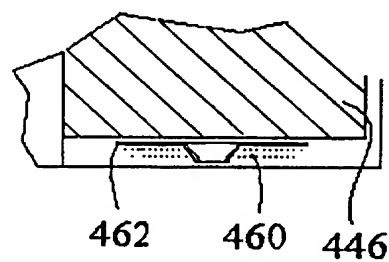
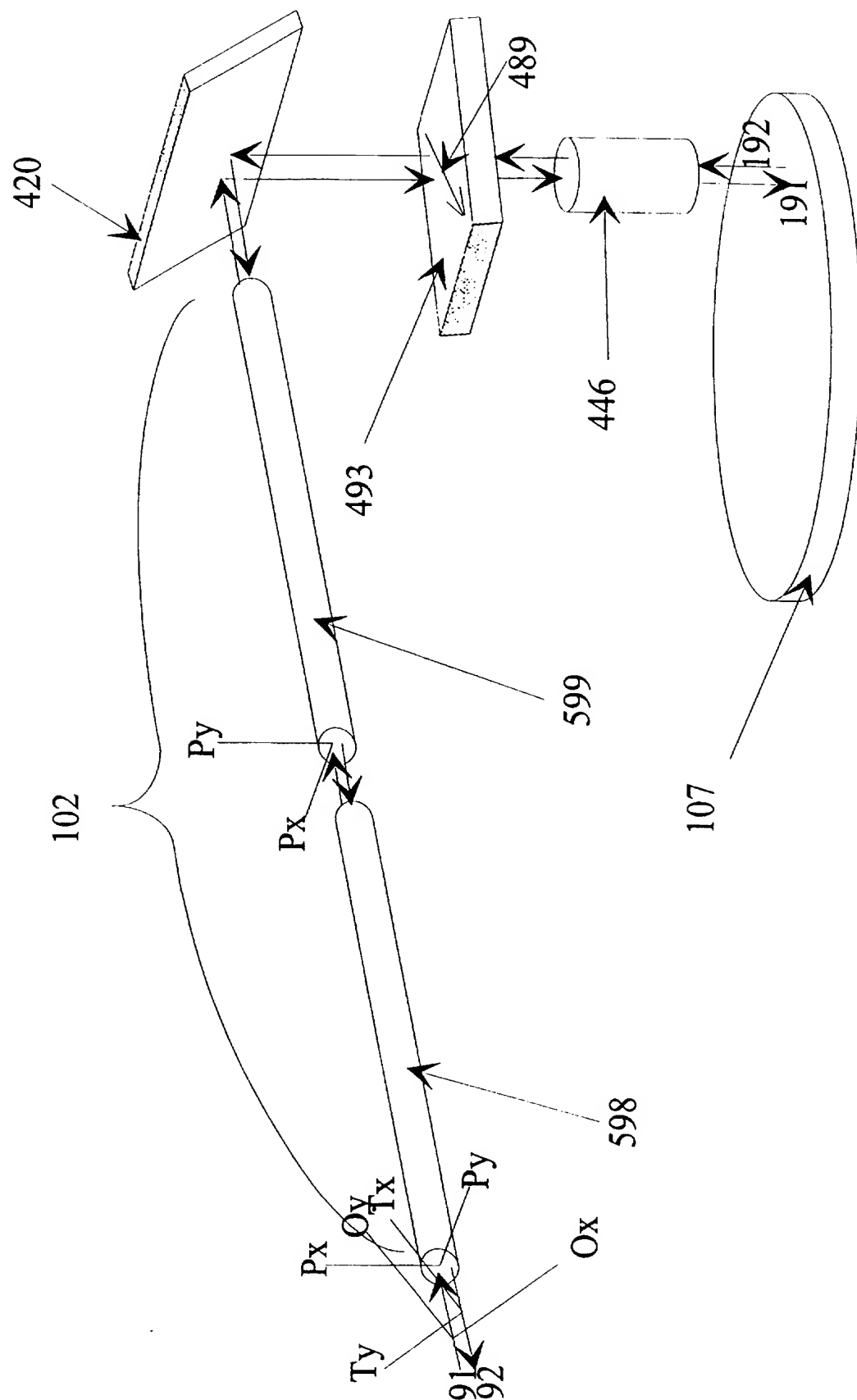


FIG. 4c

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Figure 5



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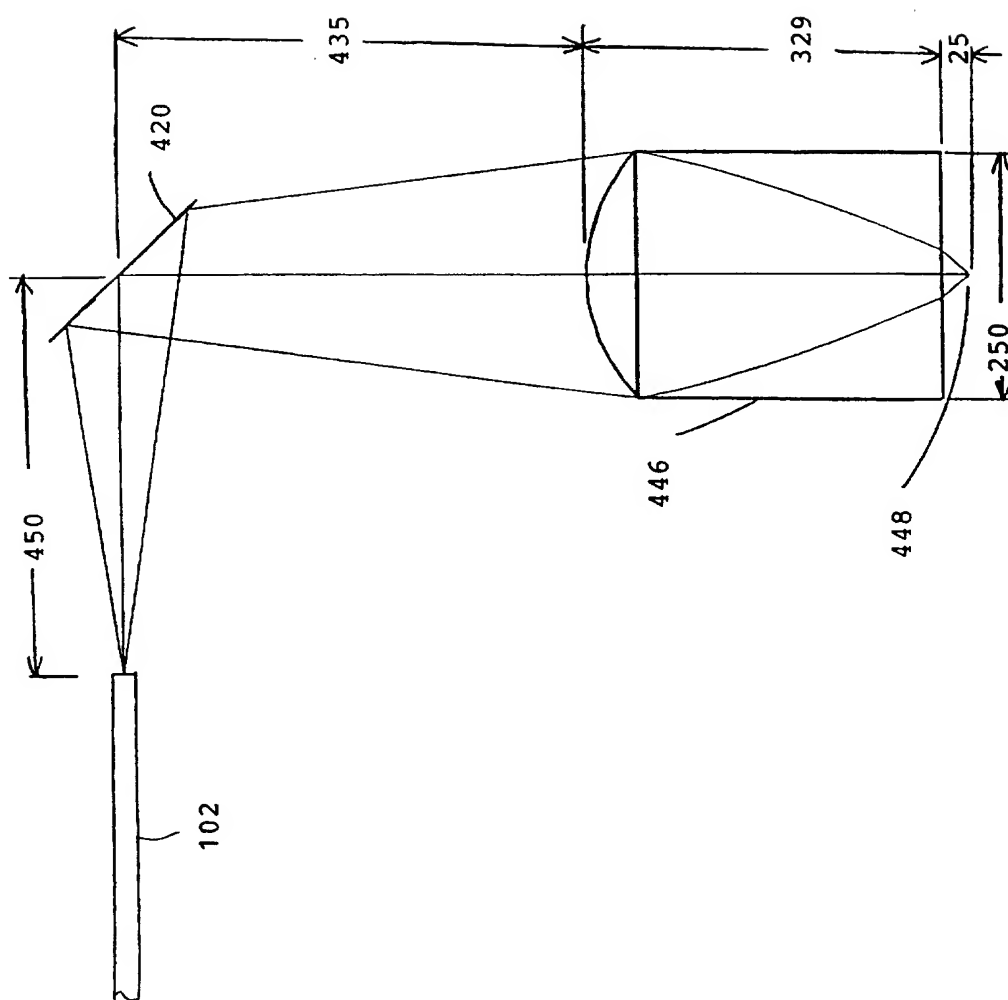


Fig. 6

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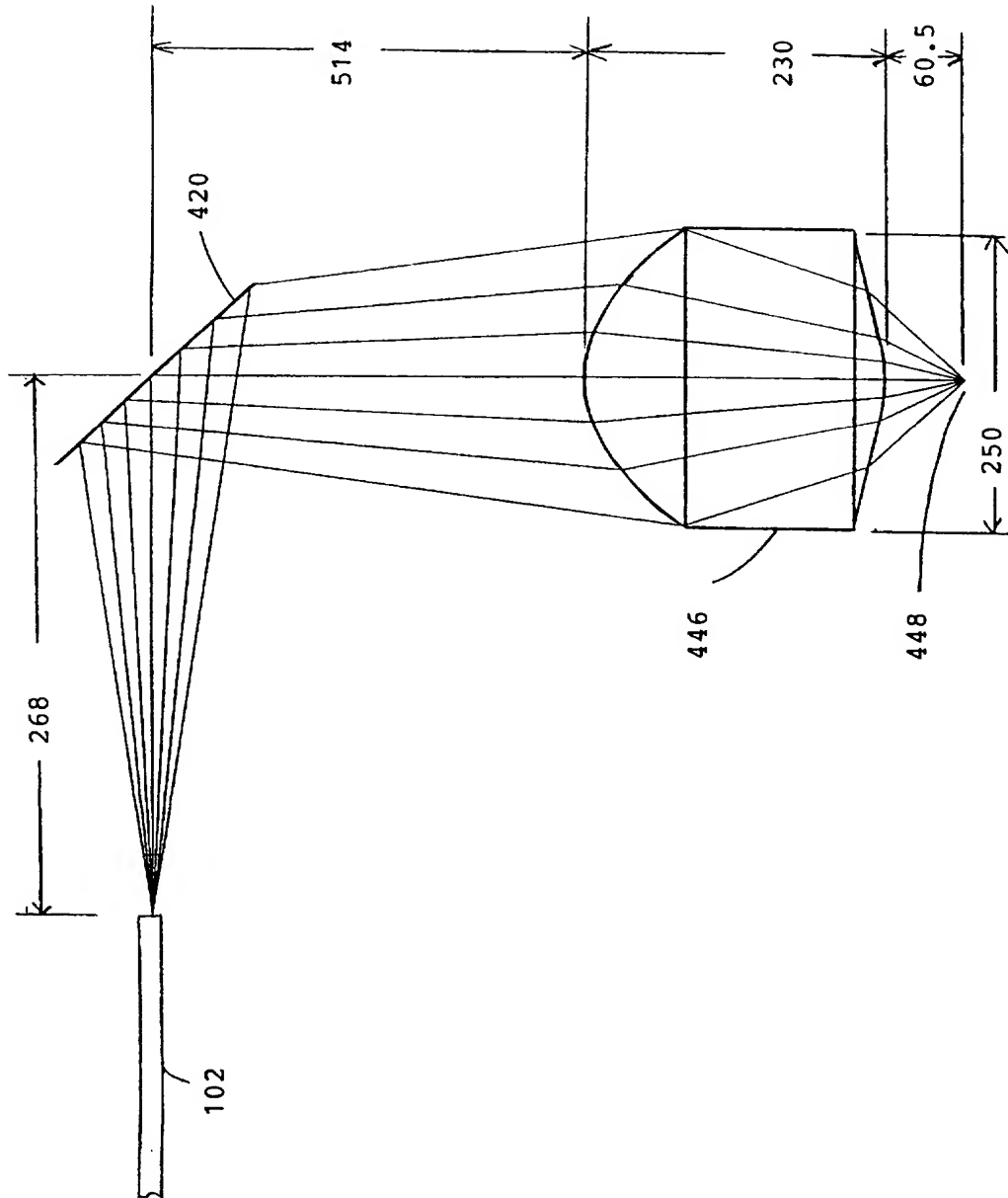
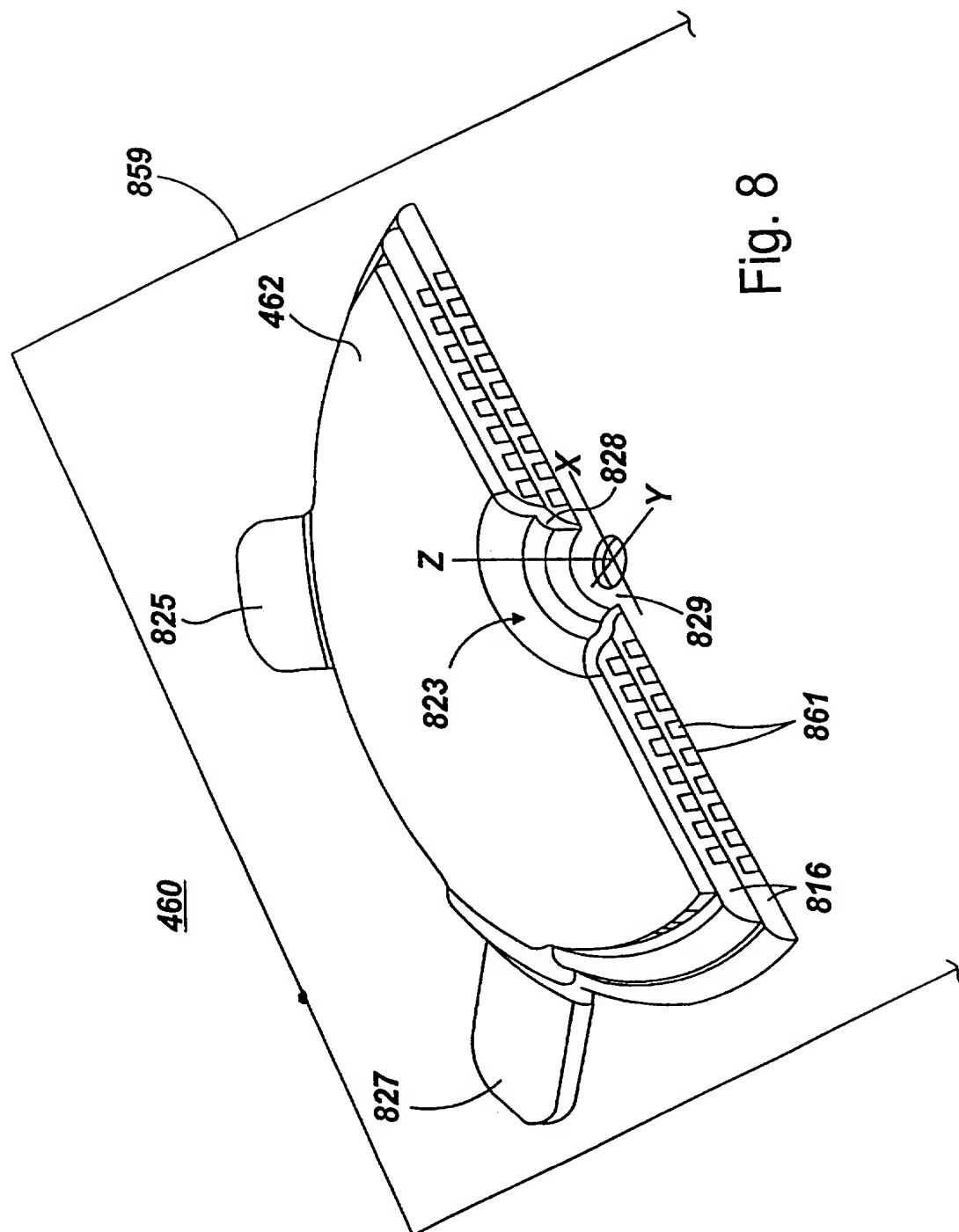


Fig. 7

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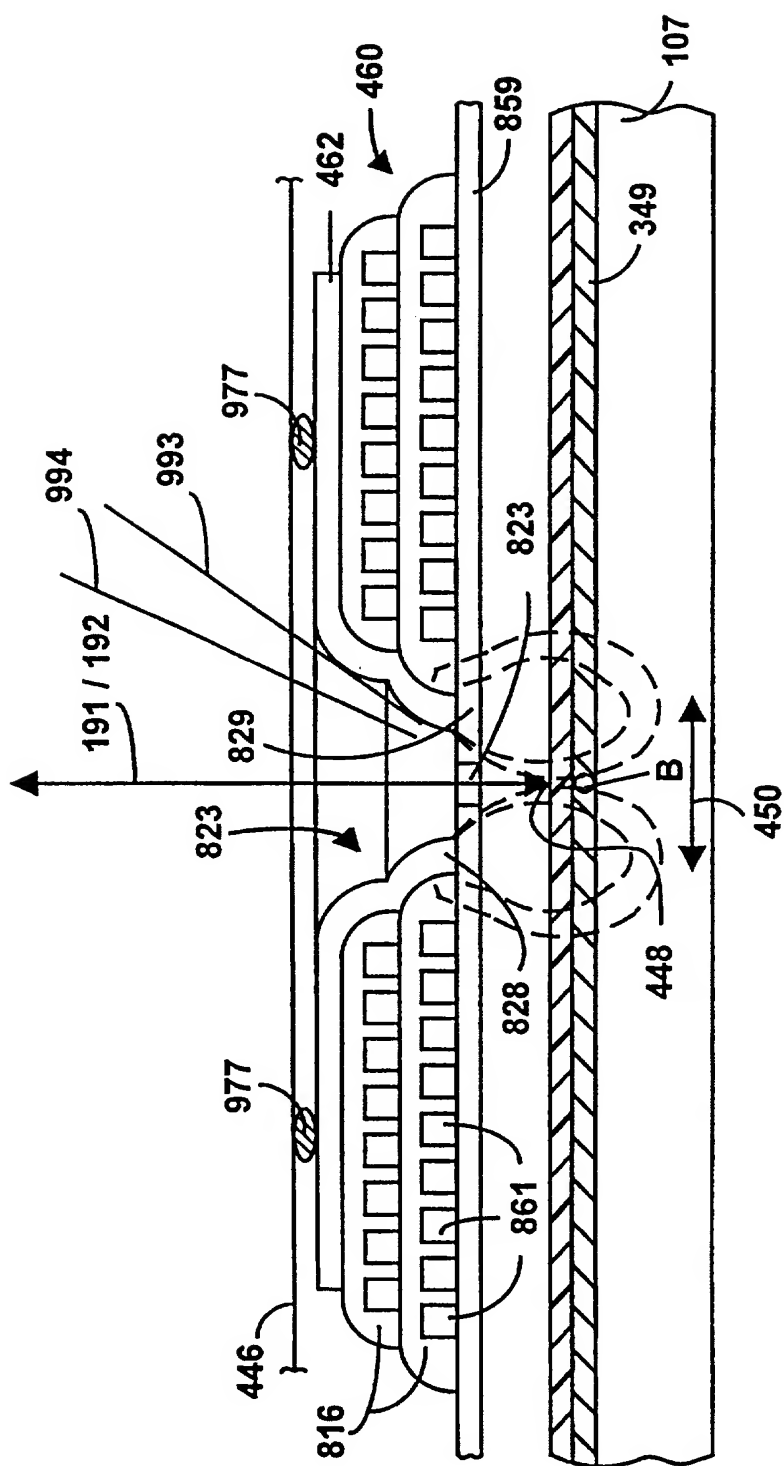


Fig. 9

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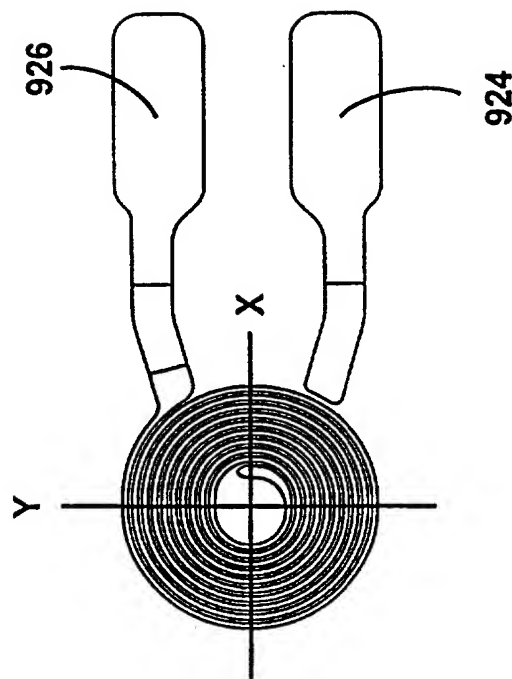


Fig. 10

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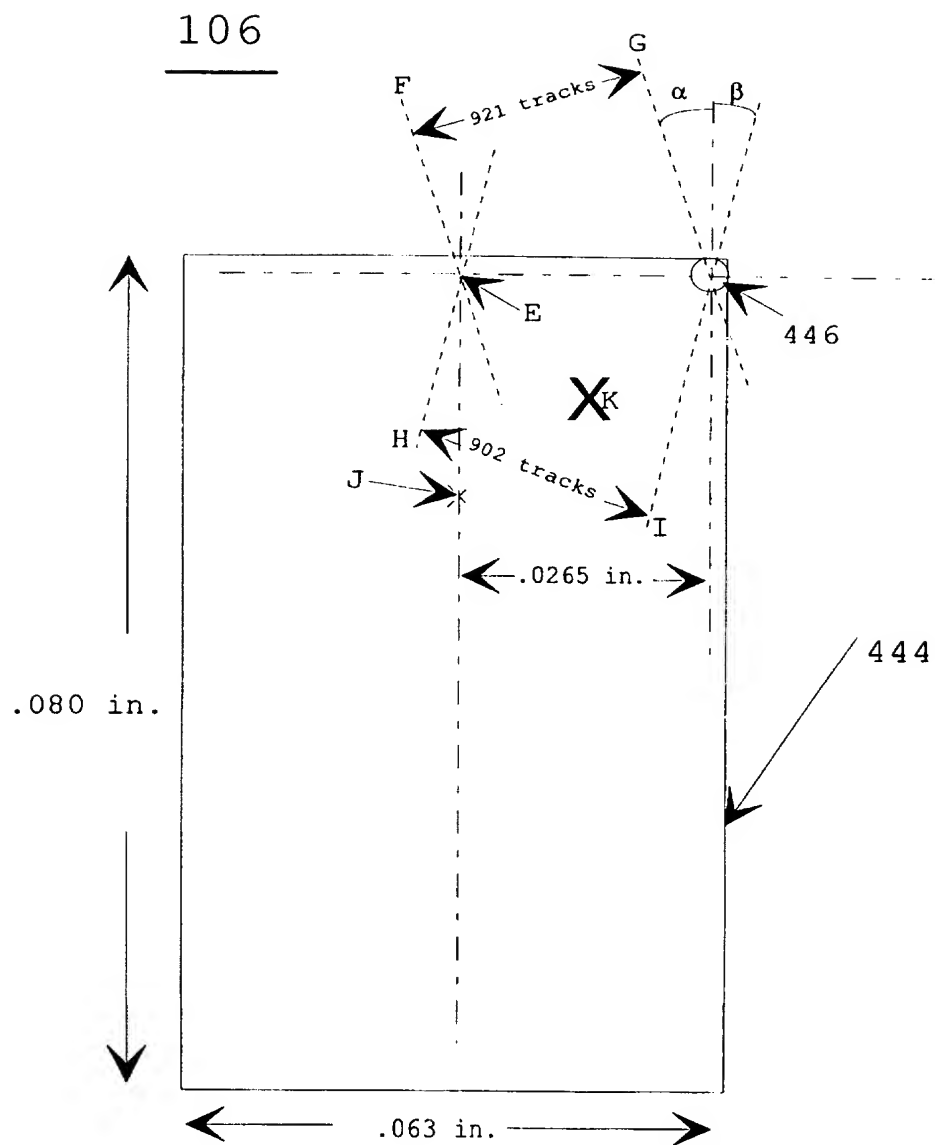


Fig. 12

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Fig. 13a

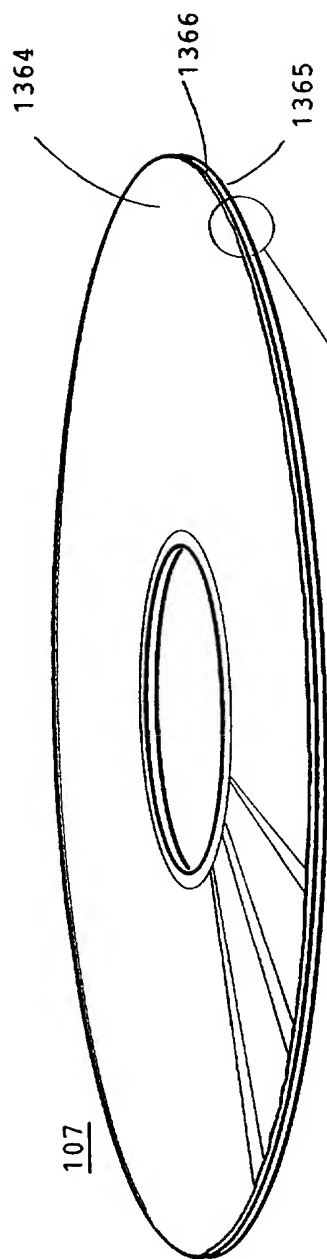


Fig. 13b

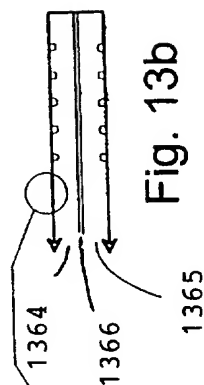
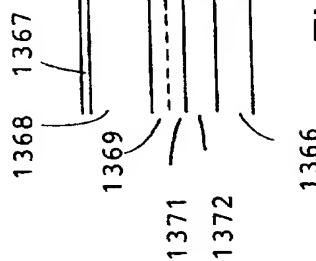


Fig. 13c



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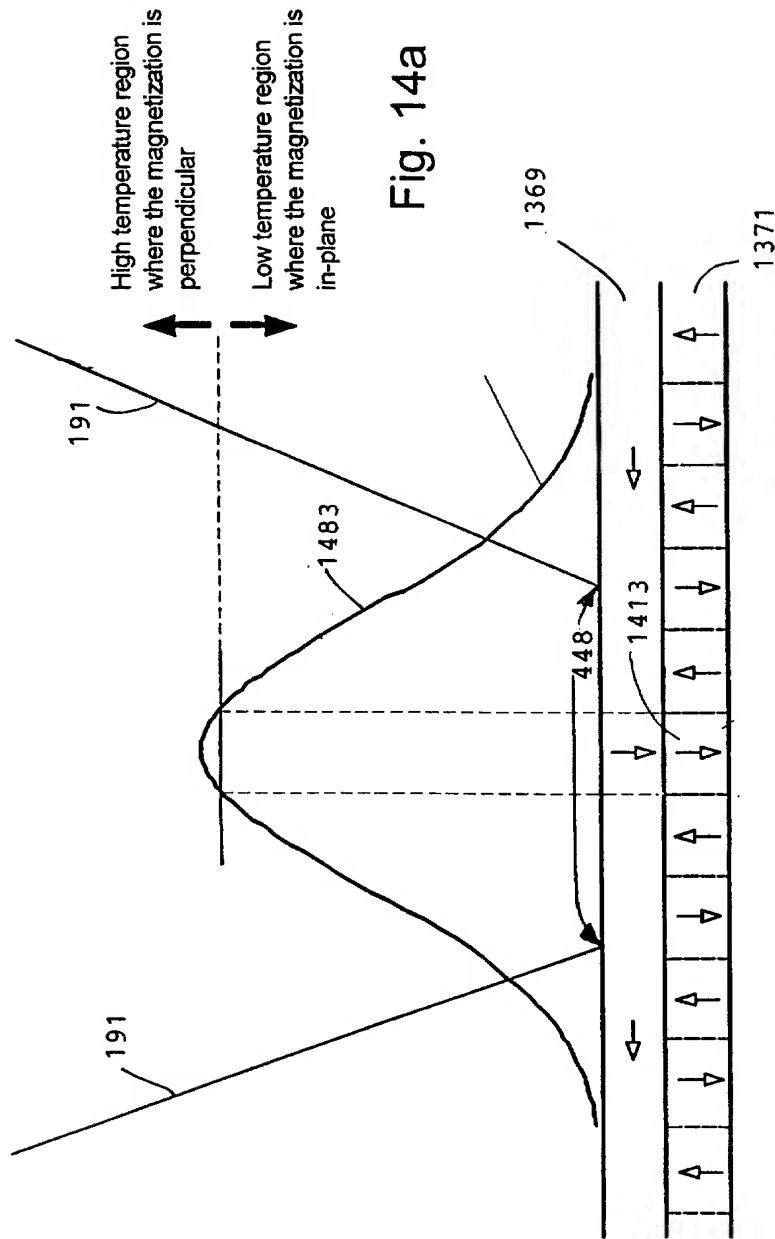


Fig. 14a

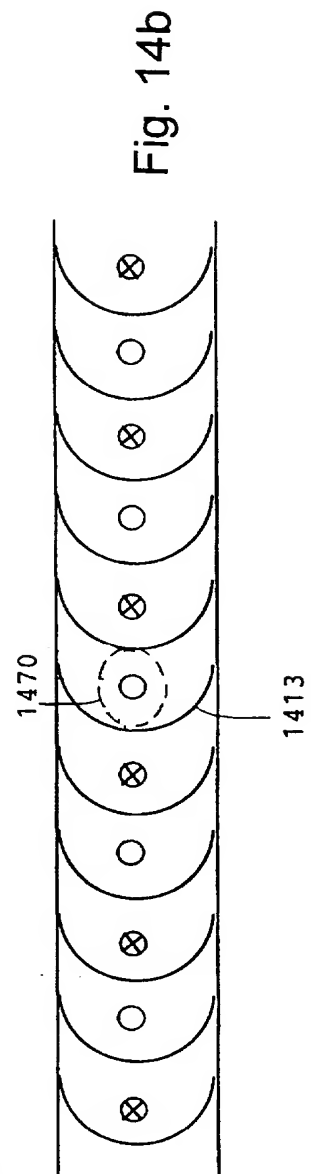


Fig. 14b

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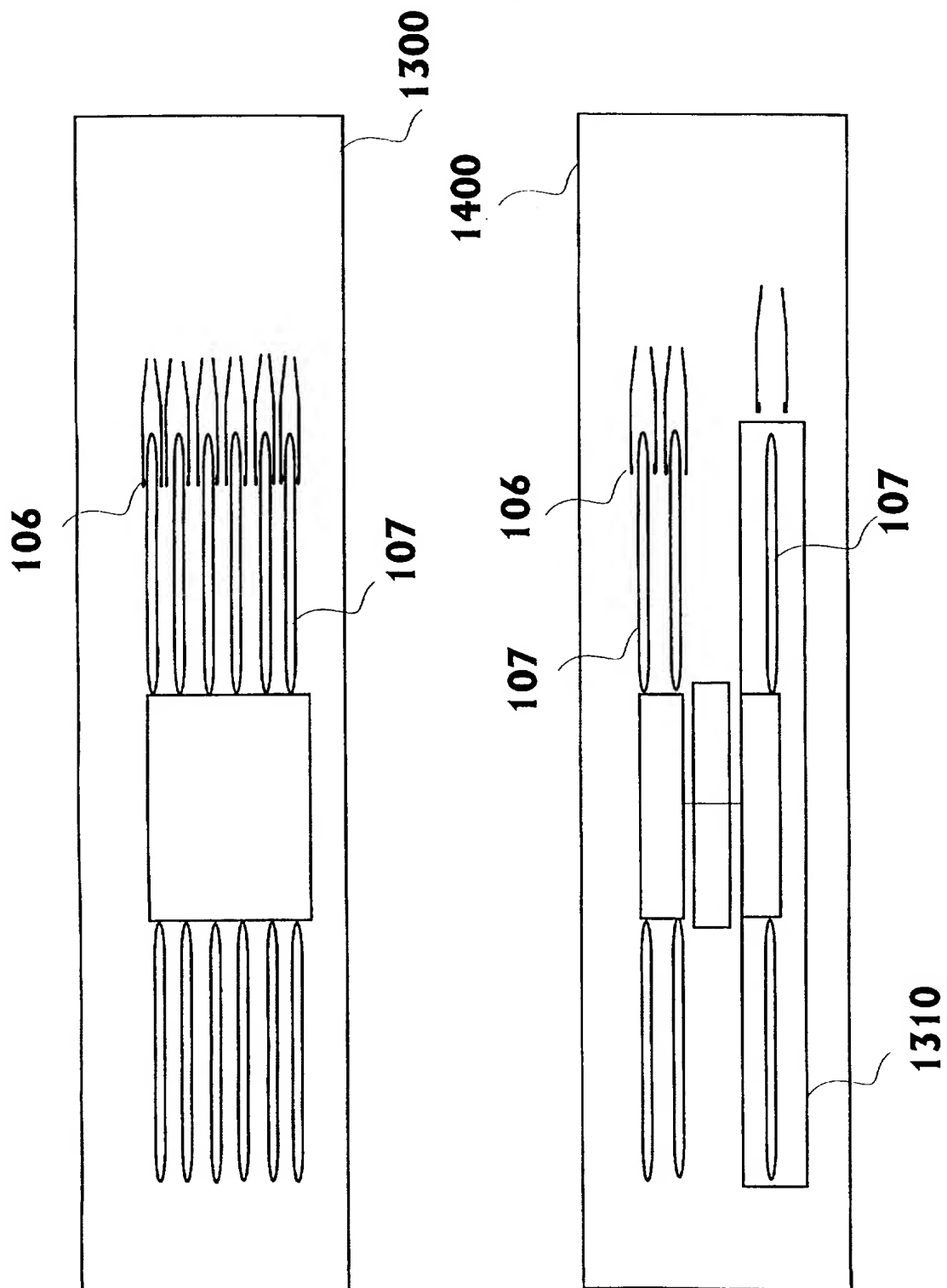


Fig. 15

INTERNATIONAL SEARCH REPORT

Intern. Appl. No.

PCT/US 97/15161

A. CLASSIFICATION OF SUBJECT MATTER

IPC 6 G11B11/10

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 G11B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	PATENT ABSTRACTS OF JAPAN vol. 017, no. 048 (P-1477), 29 January 1993 & JP 04 259943 A (SONY CORP), 16 September 1992, see abstract	1,24
A	---	35,44
X	US 5 448 538 A (ARATANI KATSUHISA ET AL) 5 September 1995 see column 2, line 1-40; claims 1-4; figures 1,4	1,24,25
A	---	35,44
A	EP 0 341 829 A (DIGITAL EQUIPMENT CORP) 15 November 1989 see column 4, line 35-50; claims 1-14; figures 1-6 ---	1-8, 37-39
	-/--	

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

30 December 1997

Date of mailing of the international search report

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INTERNATIONAL SEARCH REPORT

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PCT/US 97/15161

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5 124 961 A (YAMAGUCHI SHOJI ET AL) 23 June 1992 see claim 1; figure 17 ---	1-8, 37-39
A	EP 0 460 890 A (TEXAS INSTRUMENTS INC) 11 December 1991 see claims 1-3; figures 1,2 ---	11,12,15
A	US 5 532 997 A (PAULI GILES A) 2 July 1996 see claims 1-4; figures 1-3 ---	11,12,15
A	PATENT ABSTRACTS OF JAPAN vol. 011, no. 308 (P-624), 8 October 1987 & JP 62 099938 A (NEC HOME ELECTRONICS LTD), 9 May 1987, see abstract ---	9,14,16, 17,46
A	US 5 245 491 A (HORIE MAKOTO ET AL) 14 September 1993 see claims 1-8; figures 3-6 ---	35,44
A	US 4 460 998 A (EUGEN I. GORDON) 17 July 1984 see claim 1; figure 2 ---	35,44
A	US 5 289 454 A (MOHAPATRA SARAT K ET AL) 22 February 1994 see claims 1-6; figures 2-5 ---	35,44
A	EP 0 498 455 A (SONY CORP) 12 August 1992 see claims 1-3; figures 3-10 ---	24-33
A	PATENT ABSTRACTS OF JAPAN vol. 009, no. 170 (P-373), 16 July 1985 & JP 60 047244 A (SEIKO DENSHI KOGYO KK), 14 March 1985, see abstract ---	13,14
A	PATENT ABSTRACTS OF JAPAN vol. 012, no. 023 (P-658), 23 January 1988 & JP 62 177738 A (NEC HOME ELECTRONICS LTD), 4 August 1987, see abstract ---	13,14,16
A	EP 0 501 477 A (SHARP KK) 2 September 1992 see column 30, line 49 - column 31, line 31; figure 51 ---	22
A	PATENT ABSTRACTS OF JAPAN vol. 096, no. 012, 26 December 1996 & JP 08 212579 A (SONY CORP), 20 August 1996, see abstract ---	19
	-/--	

INTERNATIONAL SEARCH REPORT

International Application No
PCT/US 97/15161

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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